

PDN Impedance Measurements Using **Bode 500** and Picotest **PDN Probes**

13th Power Analysis & Design Symposium



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Agenda

- PDN Impedance
- Shunt-Thru Measurement Method
- 2-Port Probe vs. 1-Port Probe
- Calibration & Correction
- Step-By-Step Procedure
- Measurement Example





Power Distribution Network (PDN)

- Power source and input filters
- Voltage Regulator Module (VRM)
- Point of load regulator (POL)
- Output filtering (ferrites, capacitors)
- PCB lines, board planes, vias, capacitors
- Package leads, planes, bond-wire, on-die capacitance
- Return path (ground plane)





A Simple PDN Model



Multiple L-C resonance circuits

- Ceramic caps have generally very low ESR values.
- Ferrites have generally low resistance.
- ➤ The Q of the resonances can be high.





Impedance Profile at the Point of Load



- 200 kHz load current \rightarrow 300 m Ω source impedance.
- 3 MHz load current \rightarrow 3 Ω source impedance.
- 1 A load current causes 0.3V / 3 V drop.



Avoid Supply Impedance Peaks

- Can violate the target impedance
- High impedance increases the risk of coupling noise to the supply voltage ($V = \sqrt{P \cdot R}$)
- Noise on the supply voltage can degrade performance of oscillators (Jitter), reference voltages, ADCs, low-noise amplifiers etc...
- And in worst case, they can stack...



Risk of Rogue Waves



- Dynamic load currents at multiple frequencies can superimpose.
- Worst case scenario is a "Rogue wave".
- "Flat Impedance Approach" can safely avoid this risk.





Rogue Wave captured by Steve Sandler (Picotest)



The PDN Impedance Plot

- 1. Can be a design goal in PDN design (target impedance).
- 2. Contains information about the stability (oscillation tendency) of the voltage regulator.
- 3. Reveals resonance frequencies of the decoupling network.
- Let's measure it!
- > Challenge: Very low impedance



2-Port Shunt-Thru Measurement

- Provides high sensitivity for low impedance.
- Emulates a 4-wire kelvin connection.
- Can be used to measure into the $\mu\Omega$ range.
- Measures S21 and calculates Z via

$$Z = 25\Omega \frac{S_{21}}{1 - S_{21}}$$





Connecting Analyzer and DUT



PCB with 0402, 0603, 0805, 1206 etc. SMD Pads

VNA with Type-N coaxial connectors





P2104A One-Port Probe





P2102A Two-Port Probe





Picotest PDN Probes



- High bandwidth & flat frequency response.
- Different coaxial connector styles (SMA, BNC, N).
- Picotest PDN Cable[®] (ultra high shield attenuation and ultra low shield resistance, highly flexible and thin).
- P2102A four probe heads (0402, 0603, 0805, 1206).
- P2104A different pitch sizes available (50mil-100mil).
- 1x, 2x, 5x or 10x attenuation options available.



1-Port Probe vs. 2-Port Probe

- 1. One-Port Probe (2 probes needed 🙁)
 - 🙂 Flexible positioning
 - Get into power planes by opposite placement
 - Difficult handling (probe holder)
 - Allows measuring transfer impedance
- 2. Two-Port Probe (only **one** (1))
 - Can by used "by hand" (browser probe)
 - Very easy & intuitive to handle
 - Less flexible, no opposite placement





Measurement Setup Example



Probe & PCB clamping: http://www.clampman.info/



Setup with Bode 500 and Picotest **P2102A 2-Port Probe**

Setup with Bode 500 and two Picotest P2104A 1-Port Probes



Smart Measurement Solutions®

Ground Loop Error in Shunt-Thru Setup

VNA has common ground on source and input port

- Return current splits between source and input ground \rightarrow error voltage V_{GND}.
- Error depends on cable shield resistance, ground contact resistance, frequency (common mode inductance), DUT value [5]





Methods to Reduce Ground Loop Error

- Use cables with low shield resistance and connectors with low ground contact resistance (PDN Cables)
- Use a Common Mode Choke (J2102A or B-LCM)
 Easy to use, low impact at high frequency
 Does not work at DC / low CMRR at low frequency
- Use a Differential Amplifier (J2113A)
 - (1) Works down to DC

More impact at high frequency, limited CMRR, noisier

 Use a booster amplifier to reduce loading of VNA signal source (can reduce device internal crosstalk)



Identify the Ground Loop Error



Calibration / Correction

- Account for phase shift and attenuation of:
 - Common mode isolator
 - Cables & Probes
- Partially compensate for ground loop error (depends on ground resistance can be different from contact to contact!)

Bode Analyzer Suite offers:

- Full-Range Impedance Calibration Preferred if frequency range is unclear (uses interpolation)
- User-Range Impedance Calibration Preferred if frequencies are defined (no interpolation)





Thru or Open/Short/Load?

- Thru (Normalize S21 Measurement)
 - Only one calibration setup (thru).
 - Good signal / noise ratio during calibration.
 - \bigotimes Correction point at Z= ∞ (far from Z<<).



- **Open/Short/Load** (Normalize directly to Z)
 - Requires three calibration setups (Open/Short/Load).
 - \bigcirc Calibration includes Short (close to Z<<).
 - A perfect Short cannot be constructed.
 - BAS does not yet account for Short resistance



Add Simple Short Correction

- 1. Characterize / Model a Short (Known Short)
 - Measure dc resistance (1 A & multimeter)
 - Determine effective Short inductance (simulation or measurement)
- 2. Measure the Short & store as Memory Trace
- 3. Use an Expression Trace to Correct measurement





Measure Short DC Resistance (P2100-CAL)

1 Adc \rightarrow 0.250 mVdc Short Resistance: Rs = 250 $\mu\Omega$

Perform Thru Calibration on P2100-CAL-Thru to correct for phase shift and attenuation of cables, probe & J2102A





Save Curve to Memory and name it "SHORT"



4

Enter Expression to Correct for Short impedance $Z_{corrected} = Z_{measurement} - Z_{SHORT} + Z_{Shortmodel}$ whereby a simple model of the short could be: $Z_{Shortmodel} = R_s + j\omega L_s = 250 \ \mu\Omega + j \cdot \omega \cdot 900 \ pH$

∷ 🗹 SHORT 🕹 🏖 🛍 ≻	
🗄 🗹 Expression 1 🛛 📝 🖻 🗸	
Z{Measurement}-Z{SHORT}+250e-6+s*900e-12	
Format	Magnitude 🔹
Y _{max}	4 kΩ 🗘
Ymin	10 μΩ 🗘
Y-axis scale	Log(Y)
Expression → new memory	



Ъ

Ν.



Known 5 m Ω Resistor



DUT Connection



Smart Measurement Solutions®



P2102A + P2100-CAL Typical Values



Disclaimer: Due to my last-minute work, I was not able to confirm these values with Picotest! Values are subject to change without notice.

Ultra-Low Impedance (< $100\mu\Omega$)

- Use a Short with very low resistance (solid copper or silver)
- Suppress ground loop error as much as possible [4], [5]
- Use short cables whenever possible.
- Use cables with a low shield resistance (Picotest PDN cables).
- Measure something known of similar value.
 (1 Ω is not the same as 100 μΩ).
- Add calibration and reference elements to prototype layout. Thru-vias, short, etc.
- Use coaxial connectors.



How Low Can you Get?

Impedance values get lower the higher the processing power gets. >100 A require < m Ω impedance.

- Limit is hard to tell.
- Increase dynamics using an amplifier.
- Non-Linear control algorithms like COT cause noisy measurement. This noise cannot be overcome due to the non-linearity of the DUT.
- Noise floor of Bode 500 is $\approx 10 \ \mu\Omega$



Bode 500 Noise Floor: 1 kHz – 450 MHz

Signal Source drives Short with 16dBm, 10Hz RBW, CH2 terminated.



Example of a Lower Impedance





Picotest 256 A Demo-board with 2 x LTP8803-1A COT 48V to 1.1Vdc step down regulators. 250 $\mu\Omega$ at 1kHz. Noisy result at low frequency due to non-linear COT control mode.



Measuring PDN Impedance ≥ 3.3 Vdc

- Bode 500 Signal Source and 50 Ω input must be protected!
- Possible Measurement Methods:
 - 1. 3-Port measurement with Picotest J2111B current injector
 - 2. Shunt-Thru measurement with 2 dc-blocks Note: Use calibration to remove the impedance of the dc-block
 - 3. Shunt-Thru measurement with **Series-Resistance Note:** Use thru-calibration to remove the resistor influence





Key benefits of Bode 500

- Frequency Response Analyzer and Vector Network Analyzer in one device
- Reliable results high accuracy, high dynamic range
- Easy to use BAS controlled, USB-C, Ethernet
- Portable compact lightweight design
- mHz to 450 MHz
- Silent



Bode Analyzer Suite

- Easy-to-use
- Powerful
- Free

Bode

Recent

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About



Hands-On (Converter Stability Demoboard)



LAB

Hands-On (Converter Stability Demoboard)



Input Filter Section





Dual DC/DC Section



GND

 $\langle Z$

Load Section





1V8 PDN Impedance



Load Stepping (20 kHz & 120 kHz)

50° Phase Margin, no 2^{nd} resonance $\approx 9 \text{ mVpp}$



Load Stepping (20 kHz & 120 kHz)

15° Phase Margin, no 2nd resonance ≈ 34 mVpp





Load Stepping (20 kHz & 120 kHz)

15° Phase Margin + 2^{nd} resonance $\approx 57 \text{ mVpp}$





Summary

- PDN impedance reveals information about
 - Control loop stability
 - Resonance frequencies in the PDN network
- Measuring PDN impedance is rather simple
 - The output capacitors are nearly always accessible
 - The control loop must not be broken
- A flat impedance approach guarantees optimum damping at all frequencies
- Lower output impedance results in less noise on power rail



References and further information:

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[3] Sandler, S., Power Integrity, Mc Graw Hill Education Ltd, 2014

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[5] Dannan, B., Sandler, S., The Challenge of Measuring a 40 uOhm (2000 Amp) PDN with a 2-Port Probe – How Much CMRR is Needed?, <u>www.signaledgesolutions.com</u>, 2024

[6] Young, C., Novak, I., Simulating and Measuring Microohms in PDNs, DesignCon, 2015

[7] Novak, I., Miller, J., Frequency Domain Characterization of Power Distribution Networks, Artech House, 2007





Thank you for your attention!

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