

# Average Current Mode Control of Switch-Mode Power Supplies



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A Leading Provider of Smart, Connected and Secure Embedded Control Solutions

## Digital Control of Switch-Mode Power Supplies

Presented by Andreas Reiter

March 15<sup>th</sup> 2023



SMART | CONNECTED | SECURE



Power  
Conversion

# Agenda



Power Supply Control Modes



Average Current Mode Control Implementation



Enforced Phase-Locking Method



Summary

# Agenda



Power Supply Control Modes



Average Current Mode Control Implementation



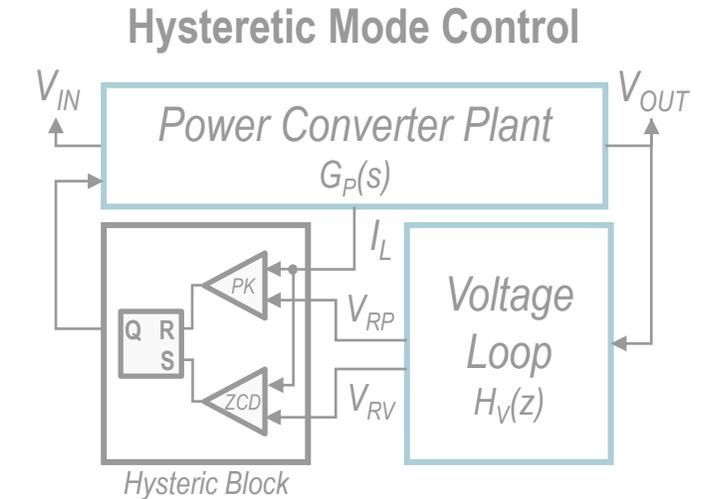
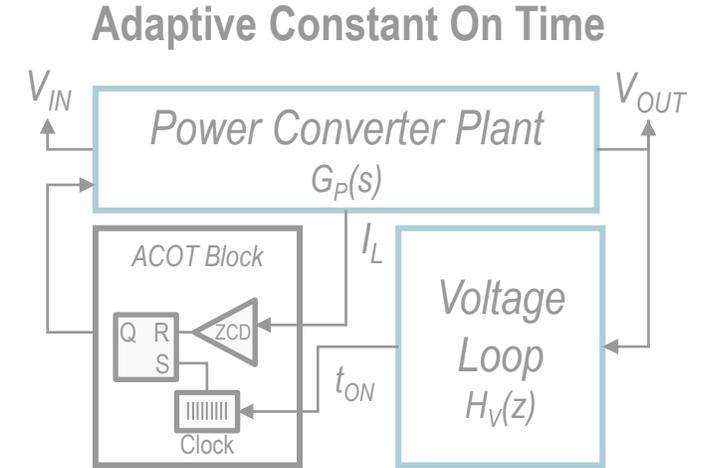
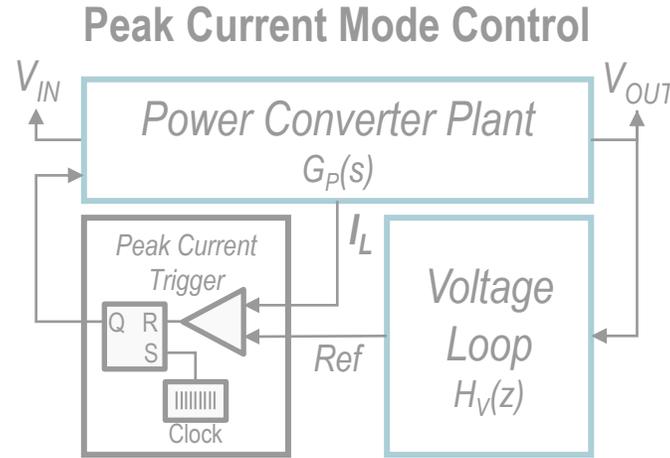
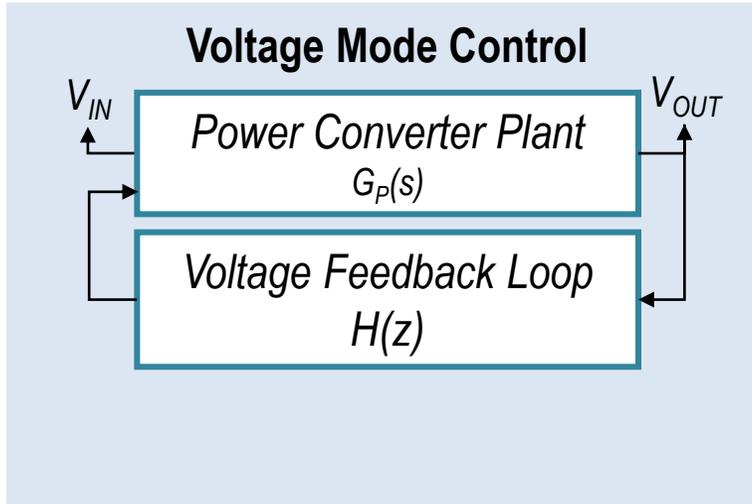
Enforced Phase-Locking Method



Summary

# Switch-Mode Power Supply Control Modes

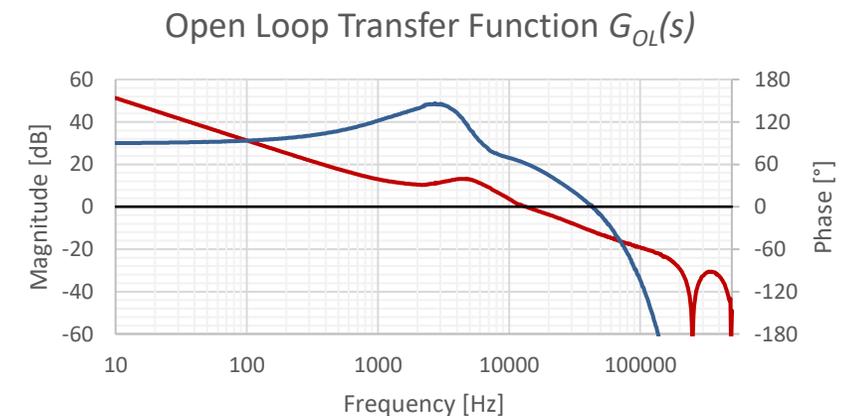
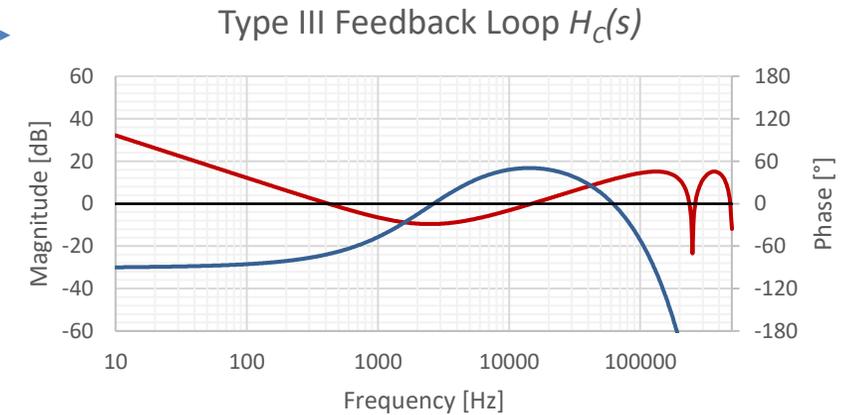
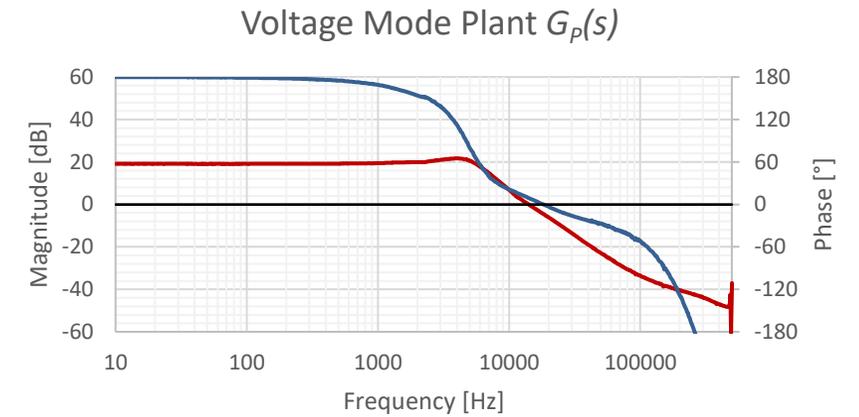
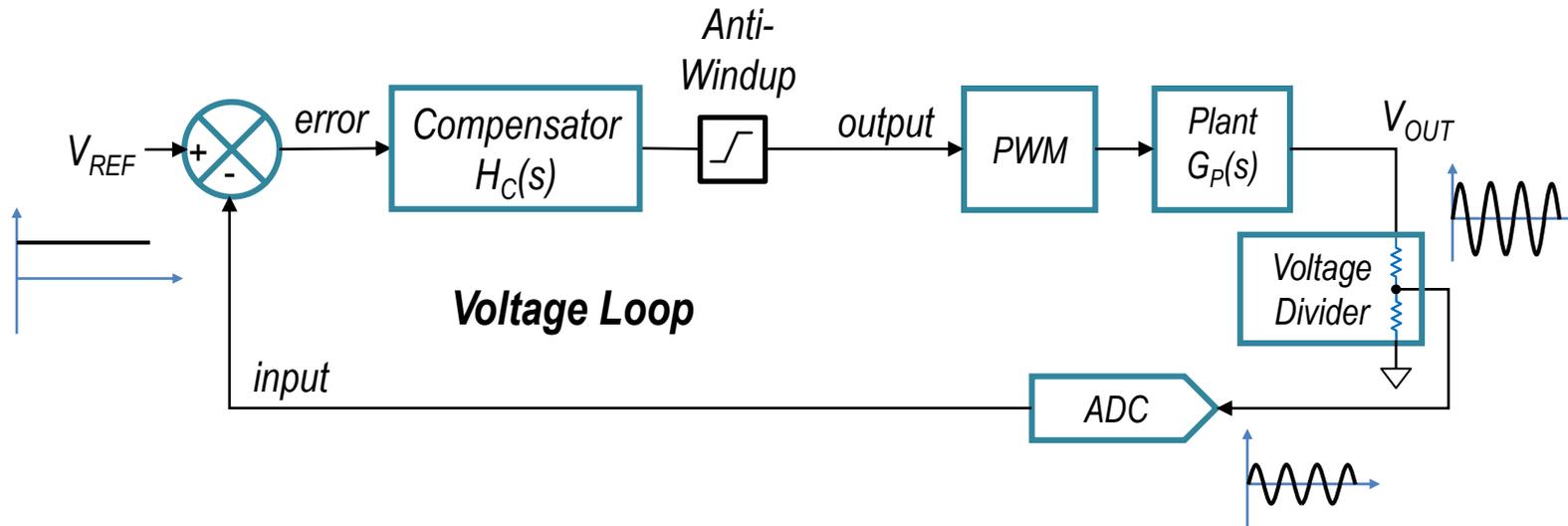
## Comparison of typical, analog feedback loop implementations



- Indirect Control Method
- Universal, Topology-Agnostic\*
- Single (uncritical) Feedback Signal
- Applicable for
  - Fixed Frequency
  - Variable Frequency
  - Phase Shift
- **Limitations**
  - Limited System Linearization
  - Varying Impedance
  - No Over Current Protection

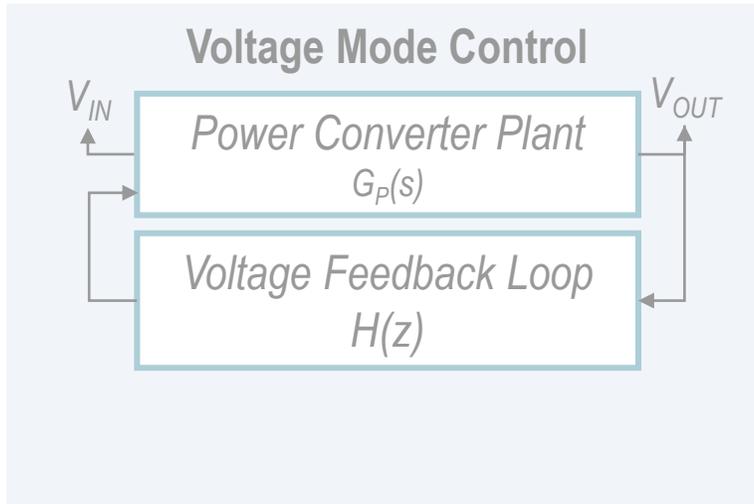
# Digital Control Scheme

## Single Voltage Mode Control Loop

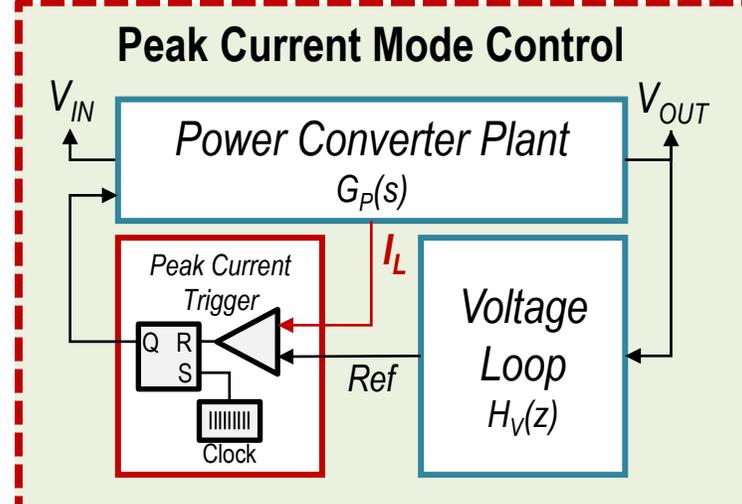


# Switch-Mode Power Supply Control Modes

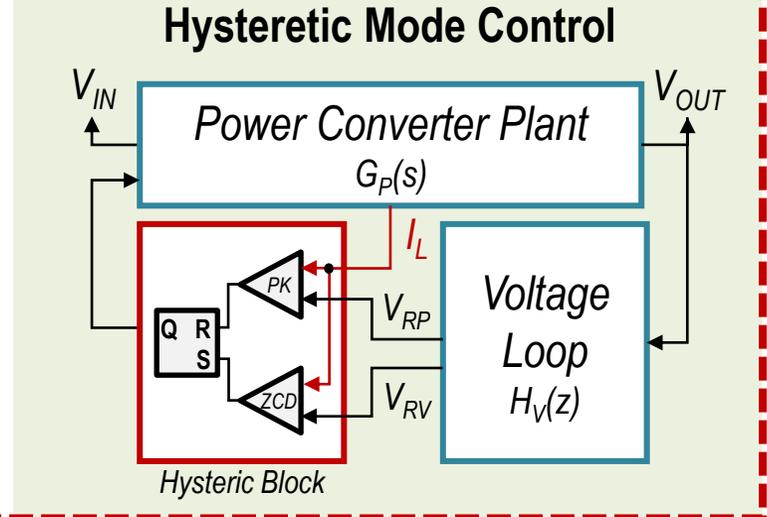
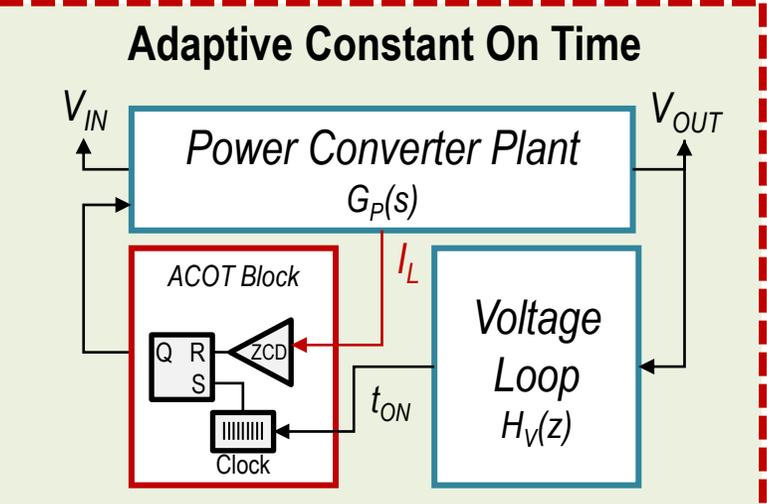
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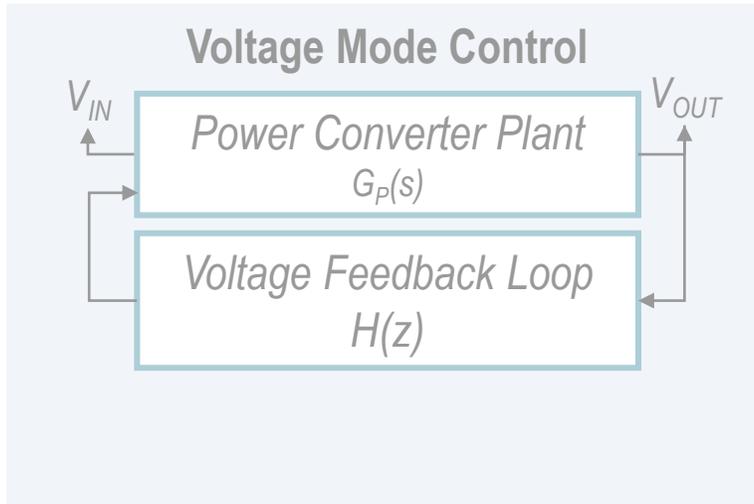


- Direct Control Method
- **Modified Switch-Node Commutation**
  - Inductor Current Control is Part of Switch Node (not the feedback loop)
- Applicable for
  - Fixed Frequency
  - Variable Frequency
  - Phase Shift
  - COT and Hysteretic Control Applicable for Variable Frequency Only

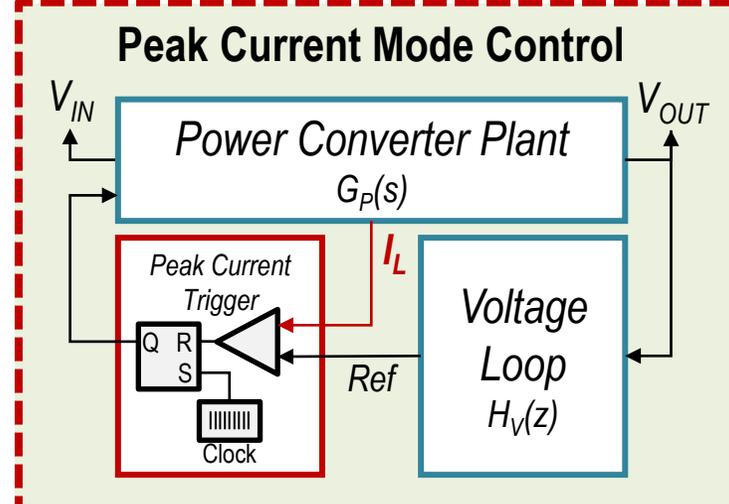


# Switch-Mode Power Supply Control Modes

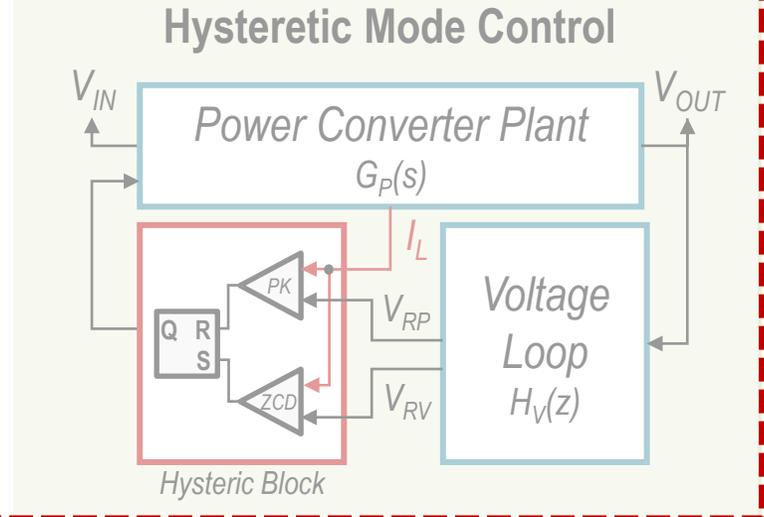
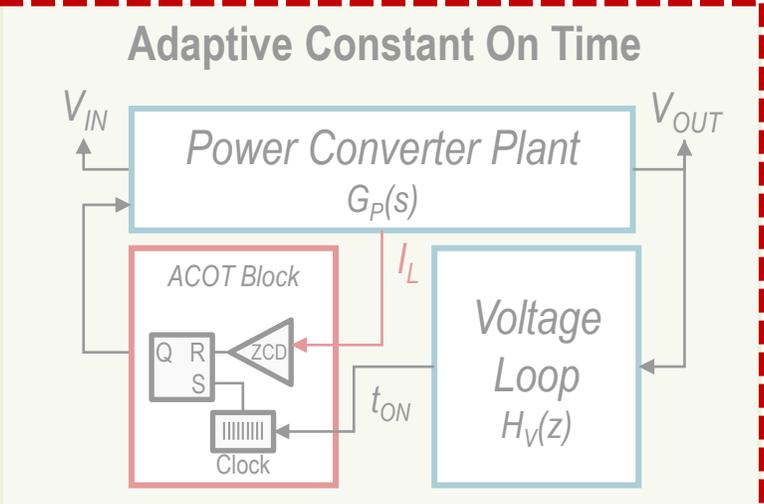
## Comparison of typical, analog feedback implementations



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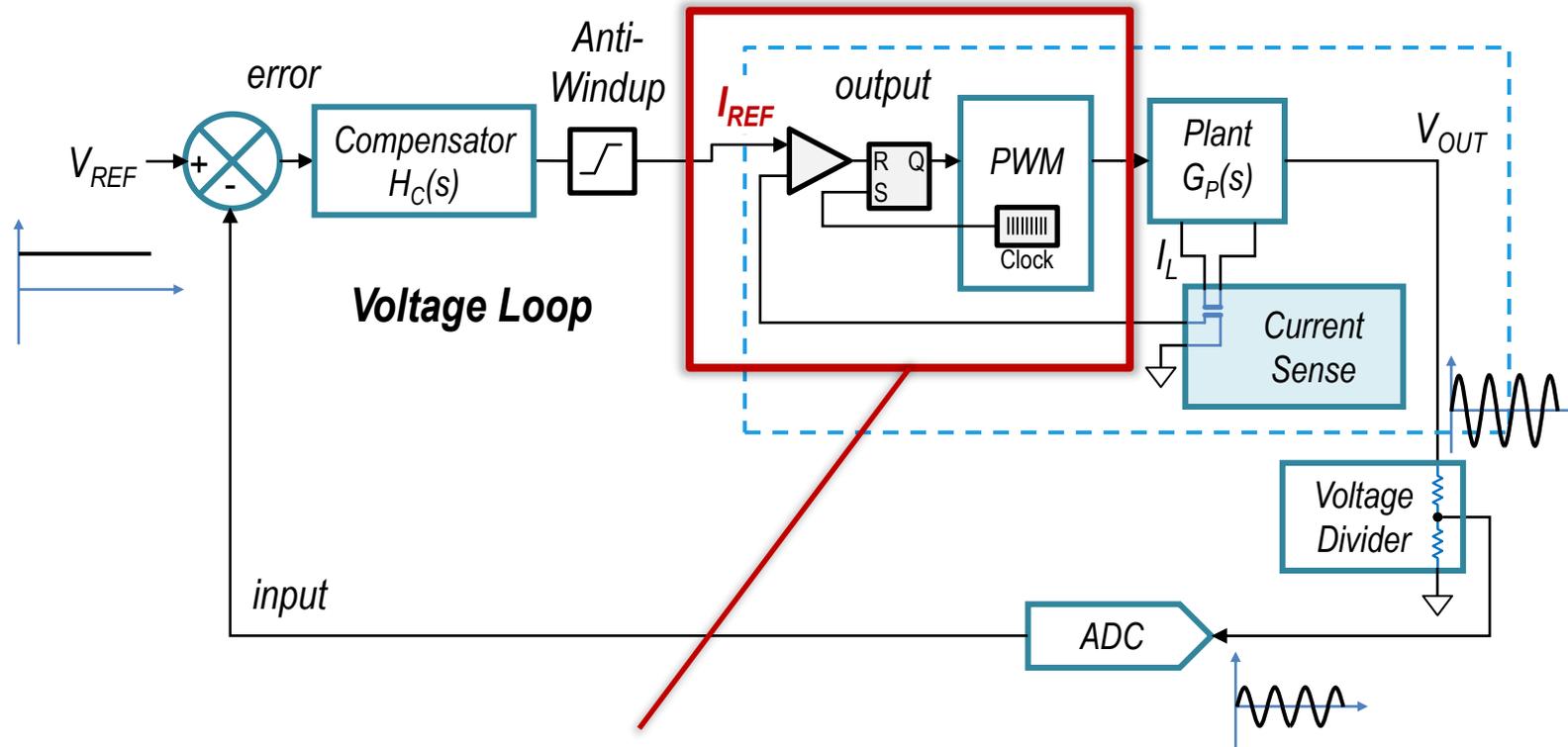


- **Direct Control Method**
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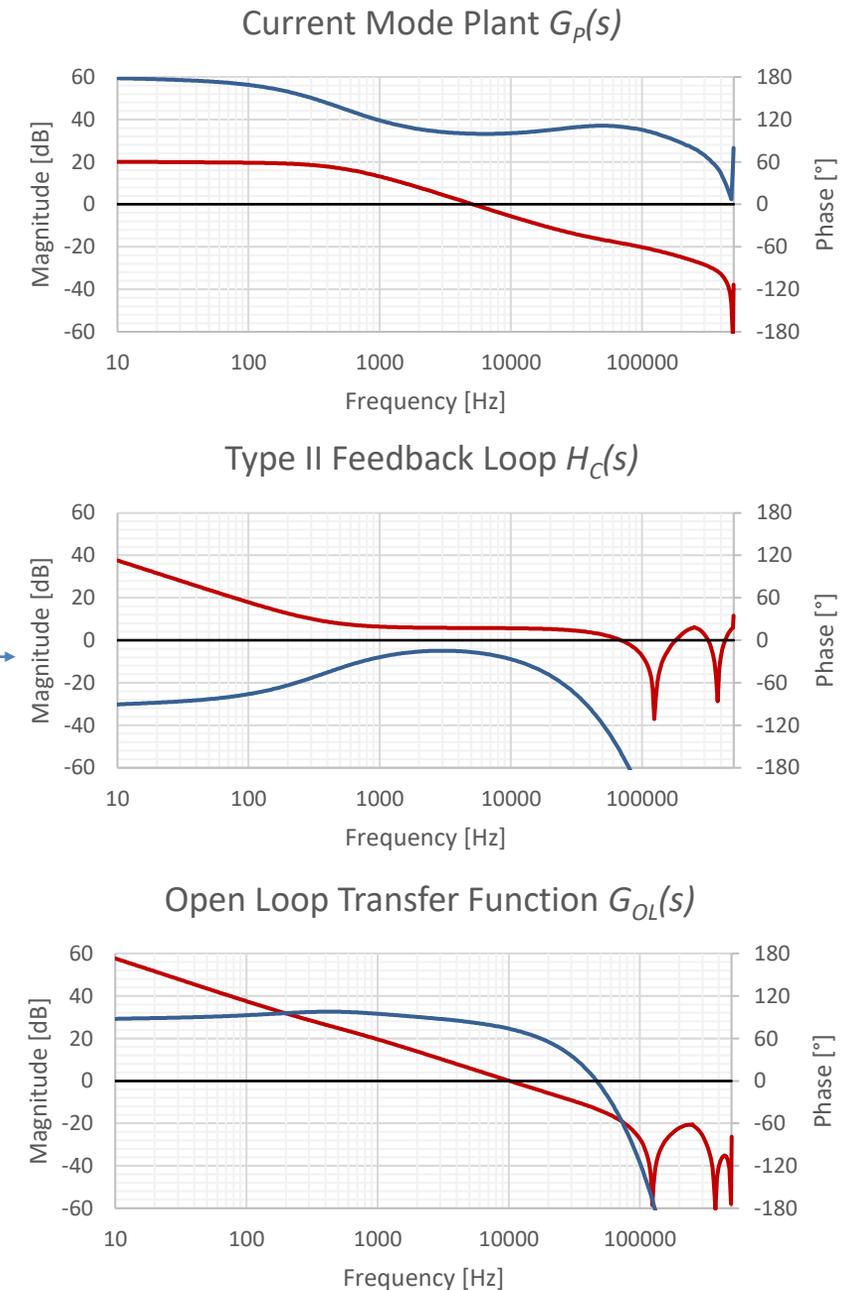


# Digital Control Scheme PCMC

## Peak Current Switch-Node Commutation

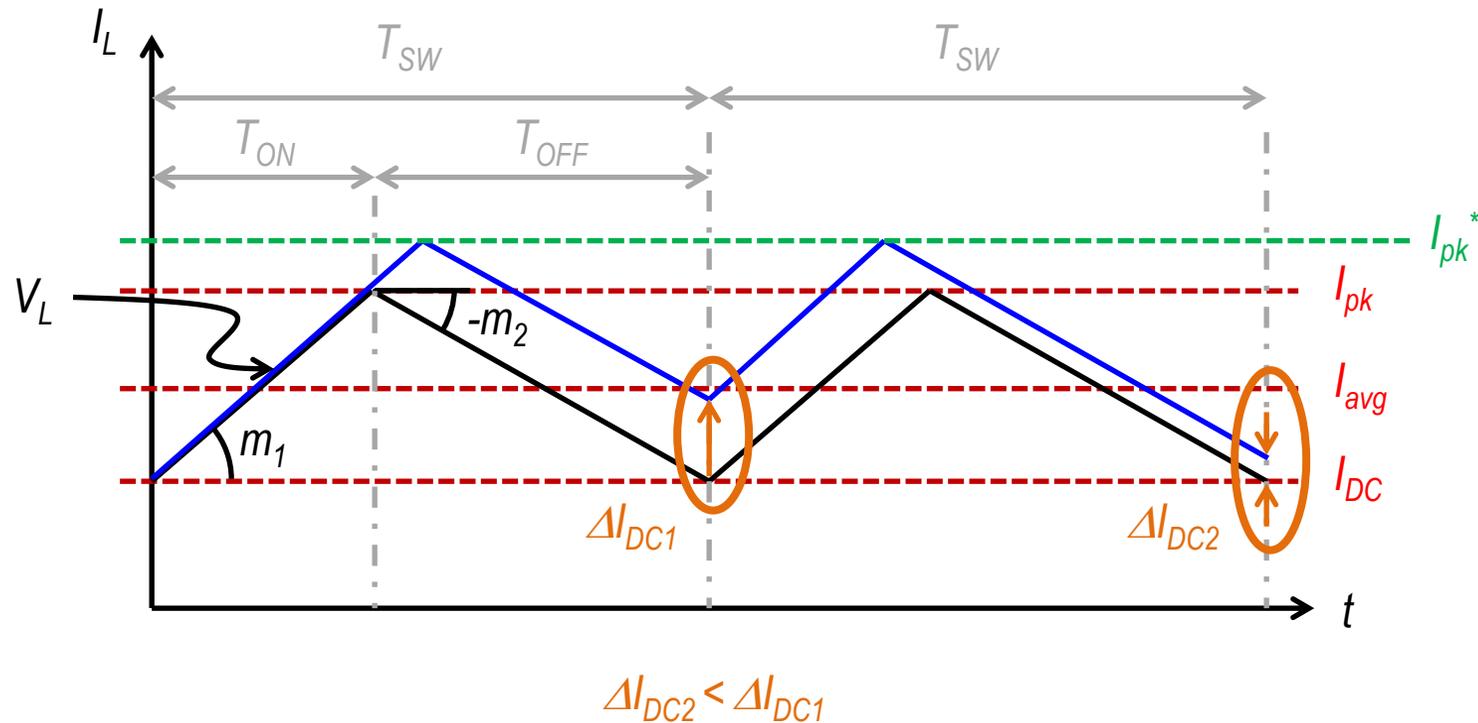


- **Unfiltered “Open Loop” Adjustment of the Inductor Current**
  - Injects Noise with every change in reference and load
  - Unfiltered PWM Signal Jitter
  - Indeterministic Current Limiting
  - Requires Synchronous Real Time Current Feedback



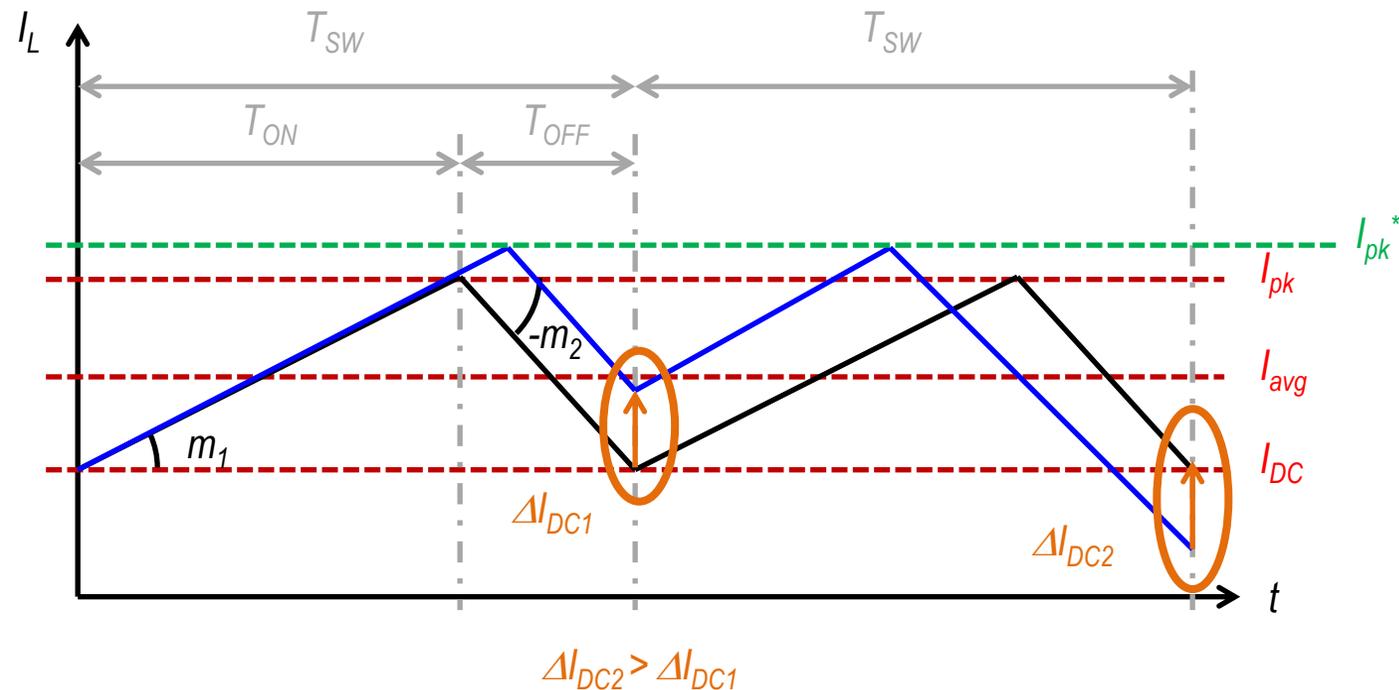
# Peak Current Modulation

Fixed Frequency Continuous Conduction Operation at DC < 50%



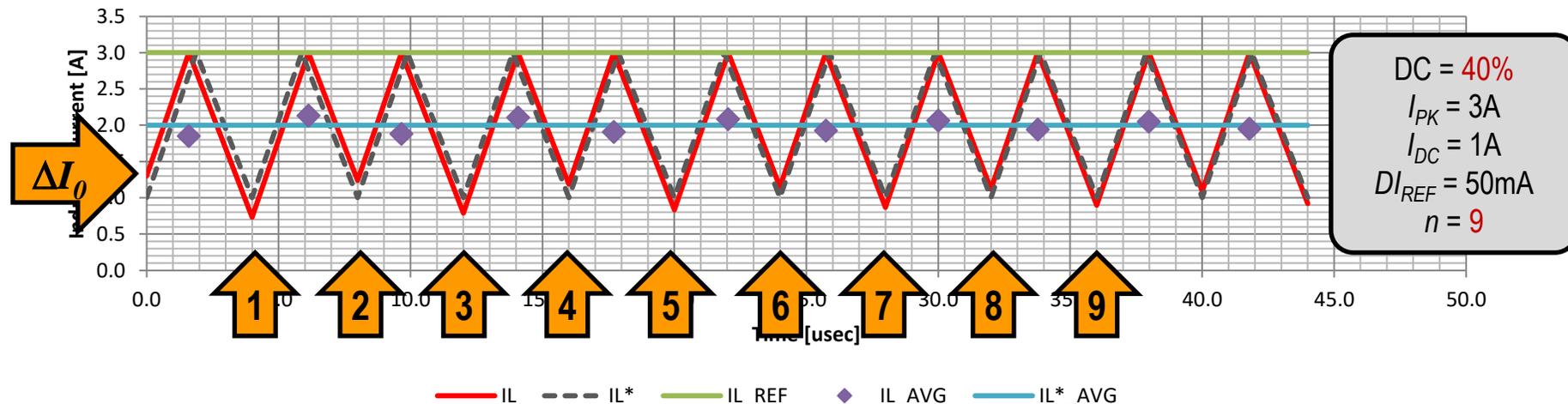
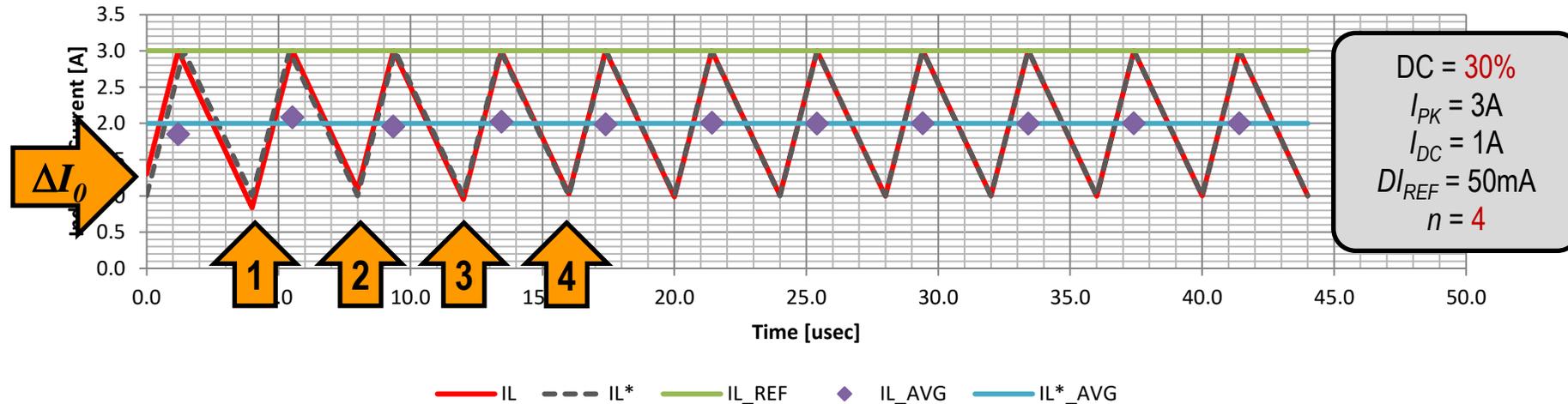
# Peak Current Modulation

Fixed Frequency Continuous Conduction Operation at DC > 50%



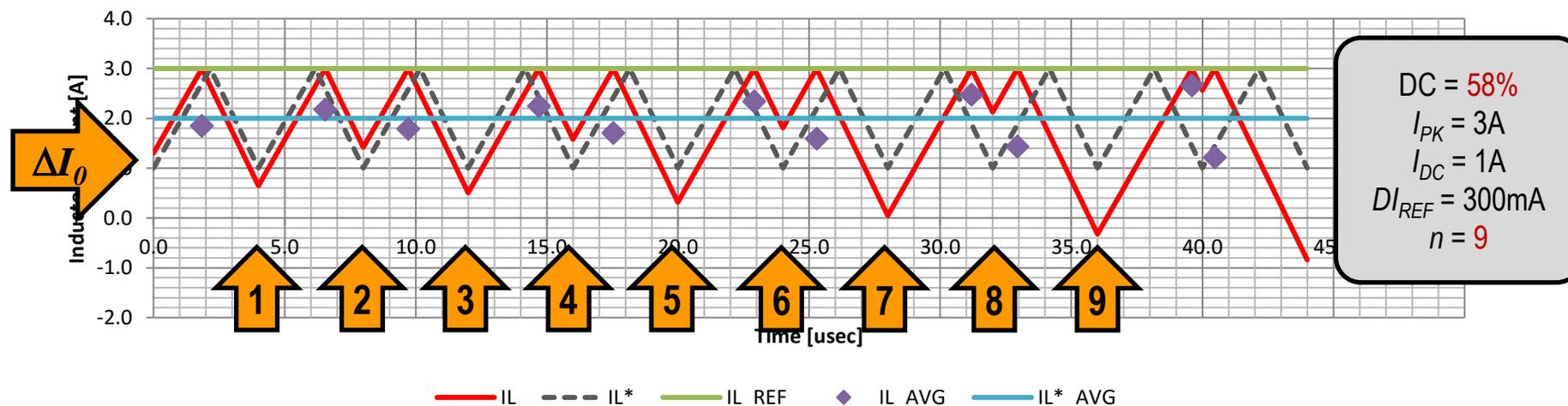
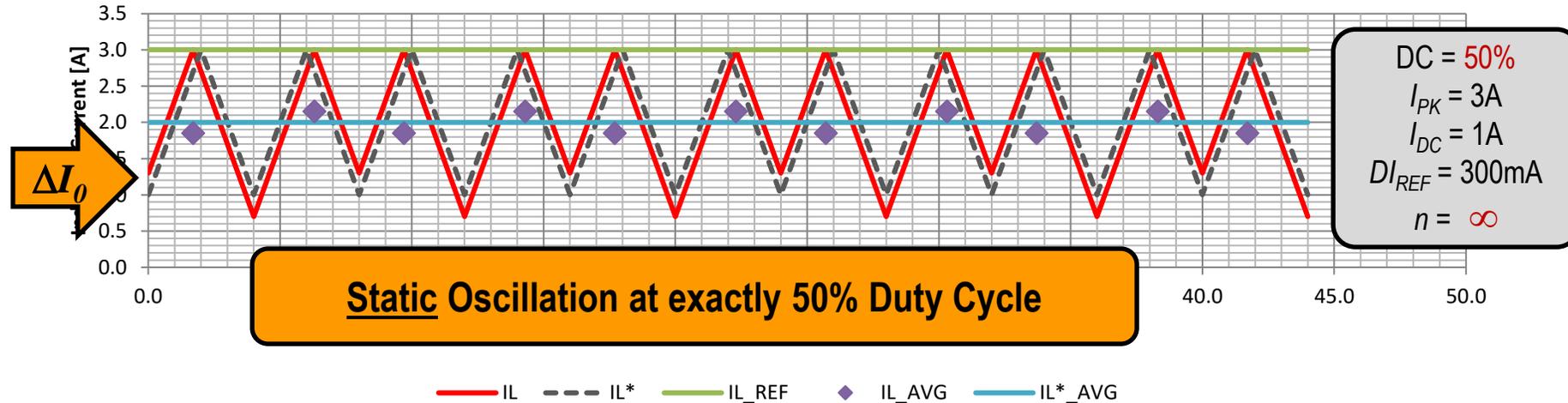
# PCMC Current Modulation

## Fixed Frequency Continuous Conduction Operation at DC < 50%



# PCMC Current Modulation

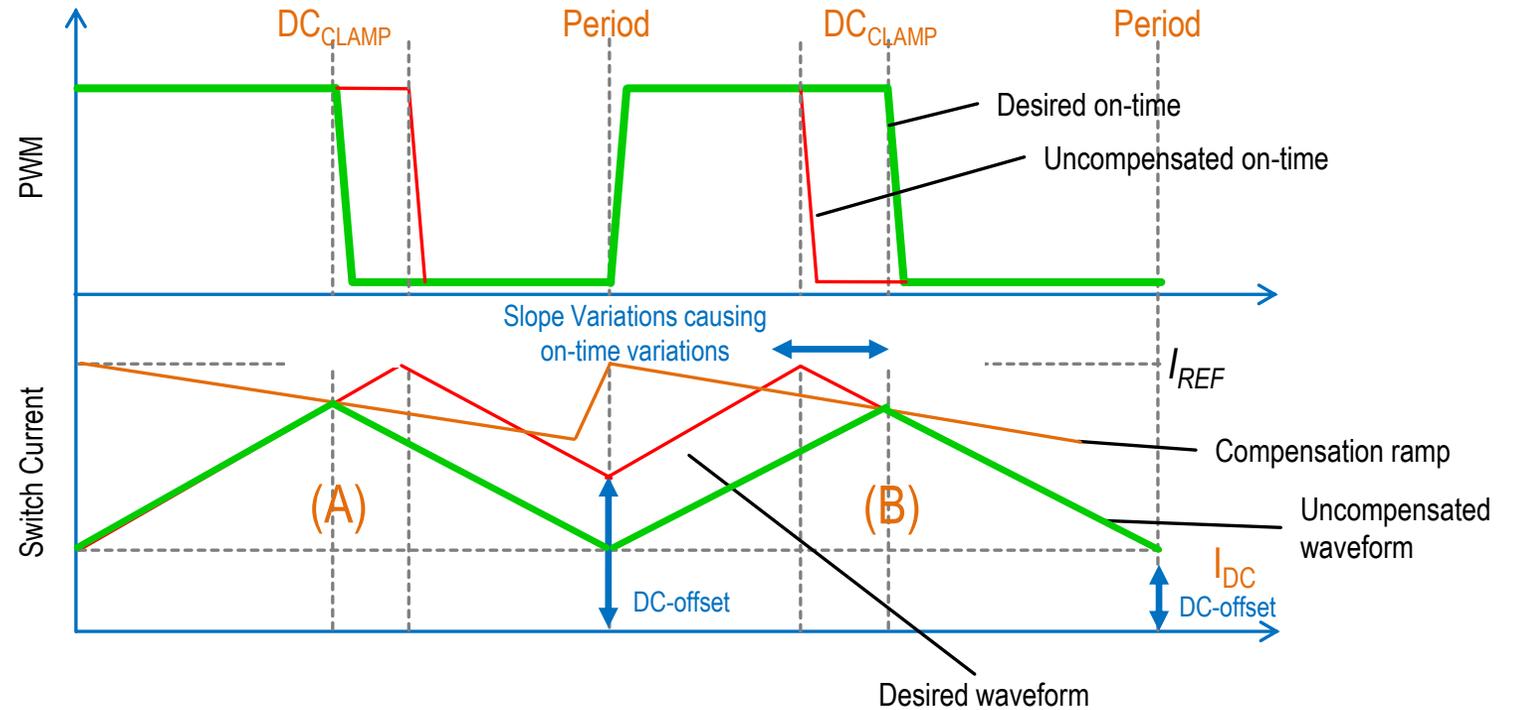
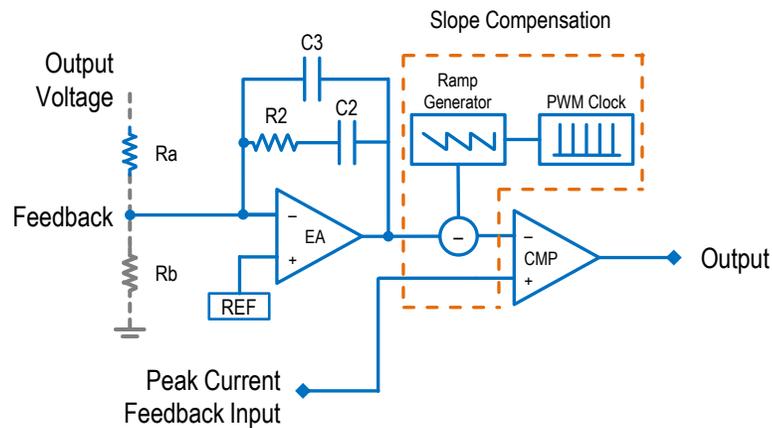
## Fixed Frequency Continuous Conduction Operation at DC < 50%



# PCMC Current Modulation

## Slope Compensation Implementation

Type II Peak Current Mode Control Compensator /w internal Slope Compensation



Response of voltage loop is slowed down with increasing duty cycle.  
Side effects: Gain variations and Voltage Droop

# Agenda



Power Supply Control Modes



Average Current Mode Control Implementation



Enforced Phase-Locking Method

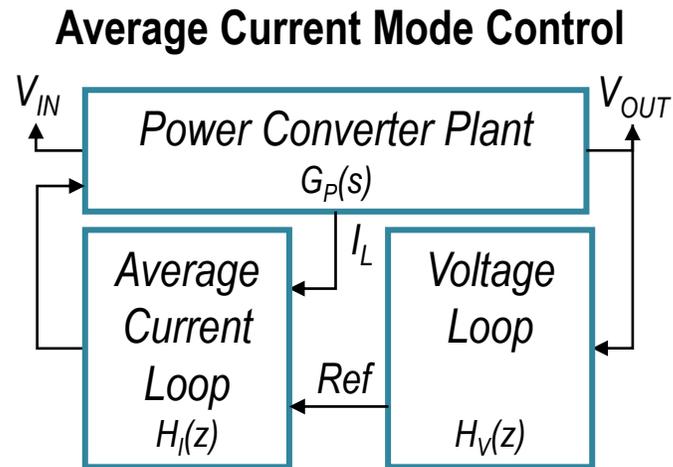


Summary

# Digital Control Scheme PCMC

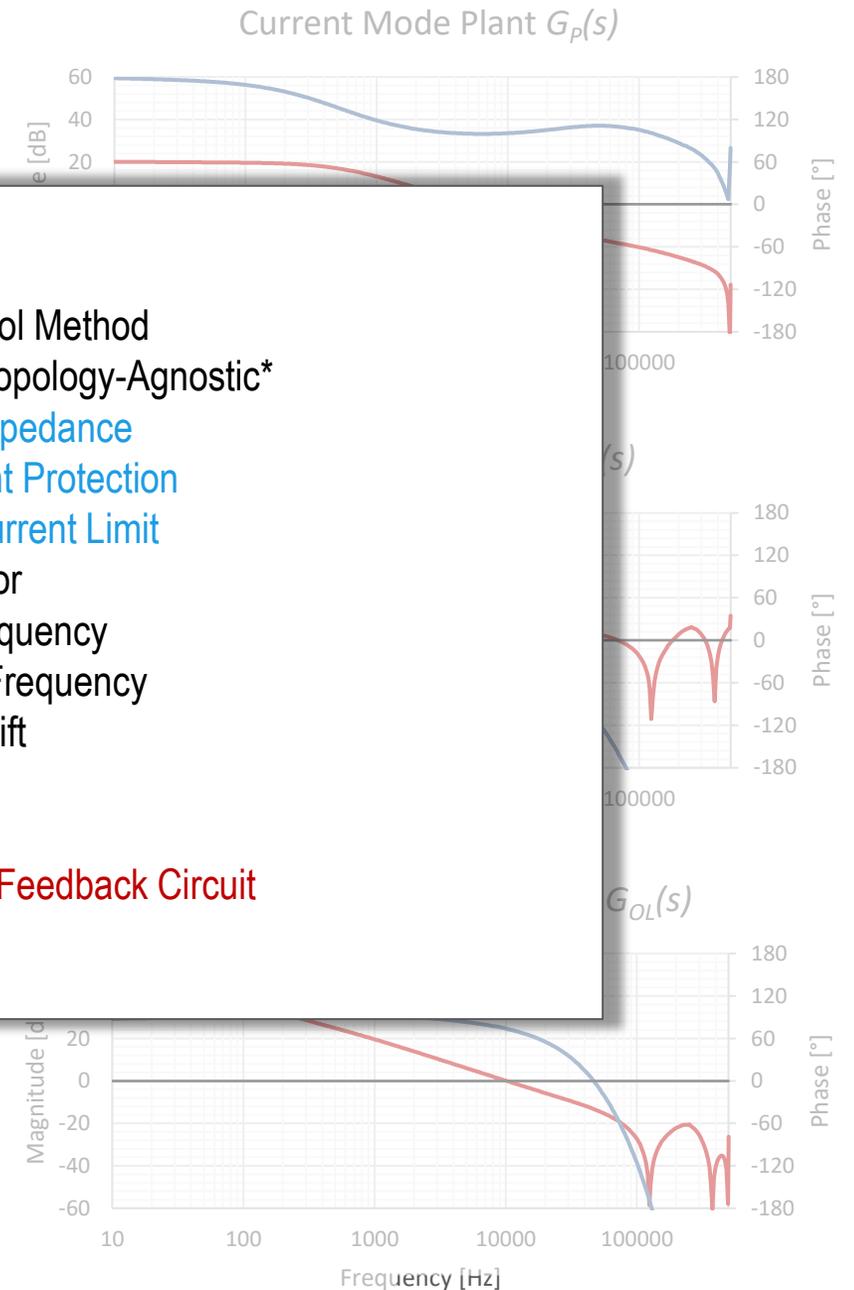
## Peak Current Switch-Node Commutation

### Solution



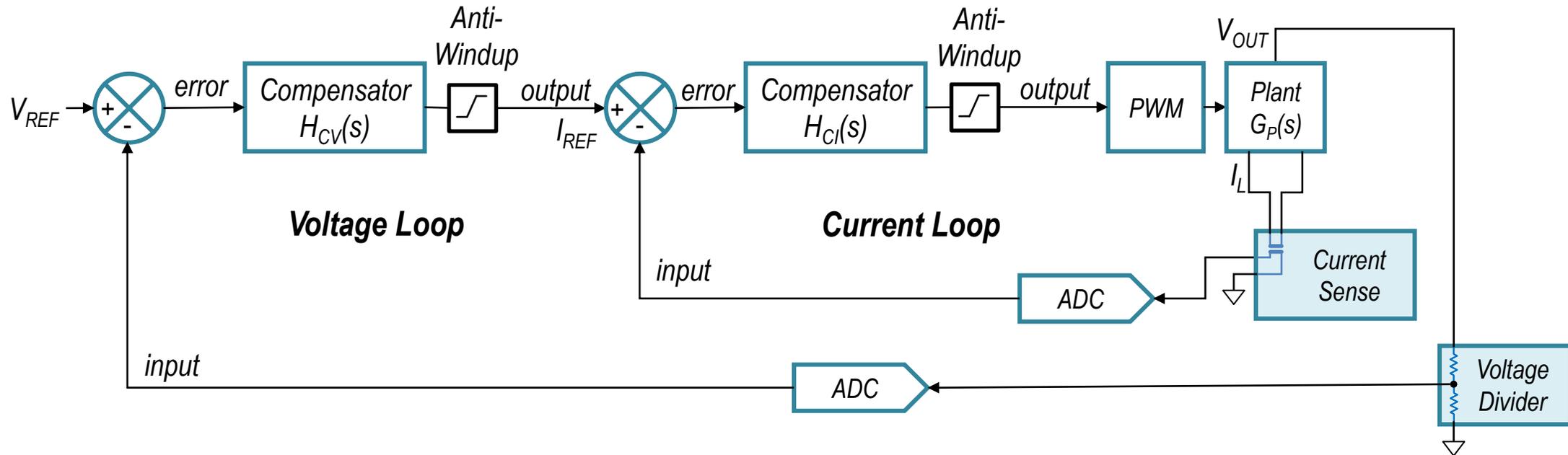
- Direct Control Method
- Universal, Topology-Agnostic\*
- Constant Impedance
- Over Current Protection
- Constant Current Limit
- Applicable for
  - Fixed Frequency
  - Variable Frequency
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- Challenges
  - Complex Feedback Circuit

- Unfiltered Open Loop Adjustment of the inductor current
  - Injects Noise with every change in reference and load
  - Unfiltered PWM Signal Jitter
  - Indeterministic Current Limiting
  - Requires Synchronous Real Time Current Feedback



# Digital Control Scheme ACMC

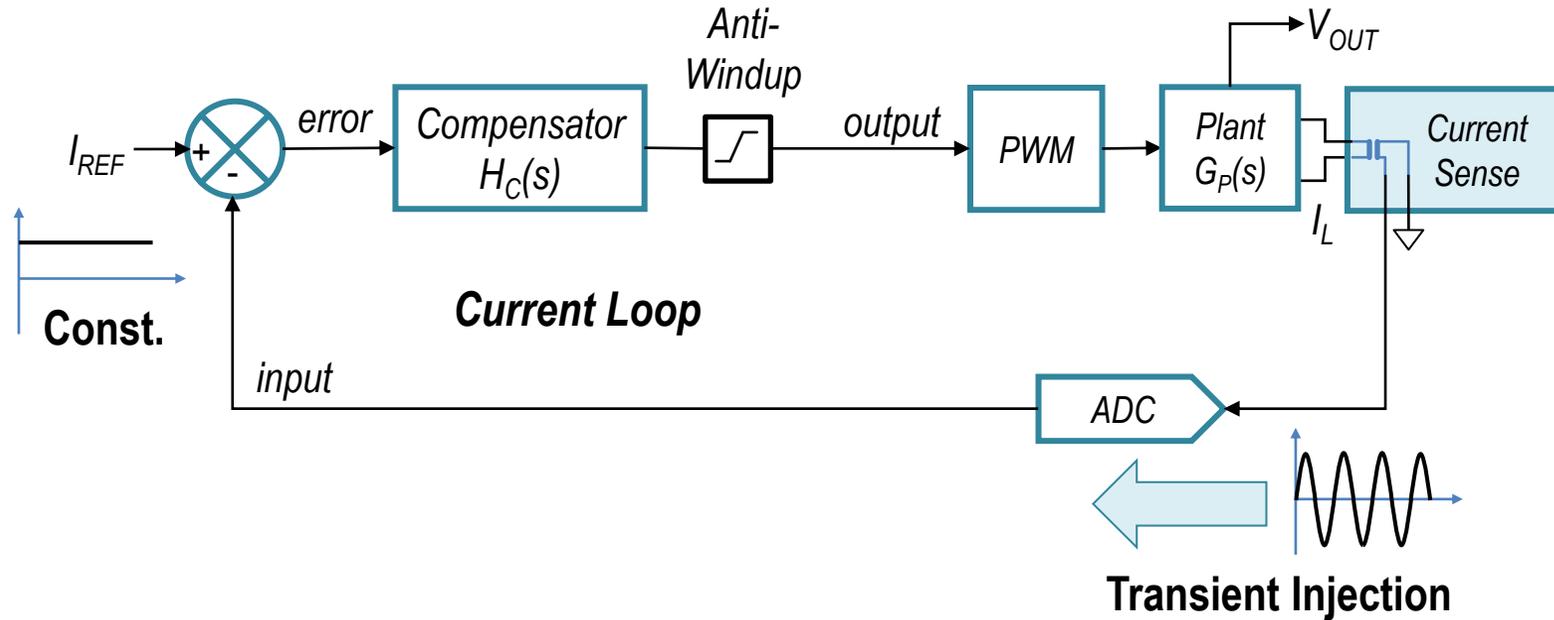
## Cascaded Average Current Mode Control Loop(s)



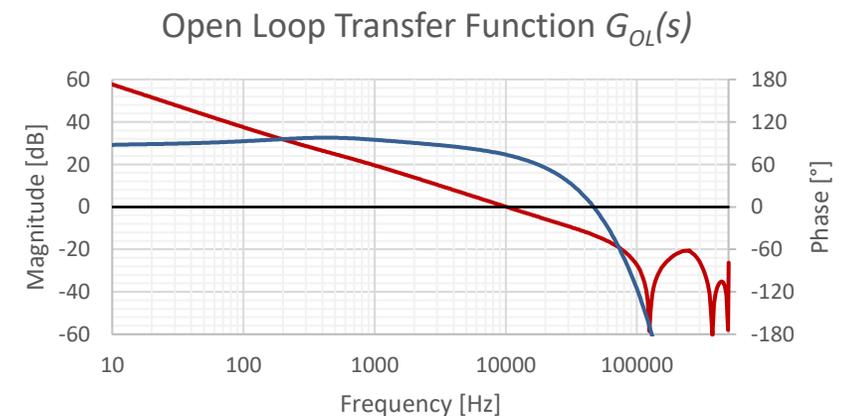
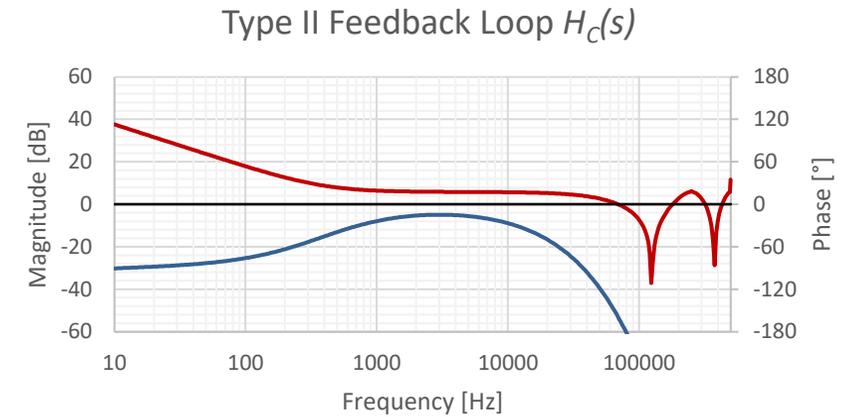
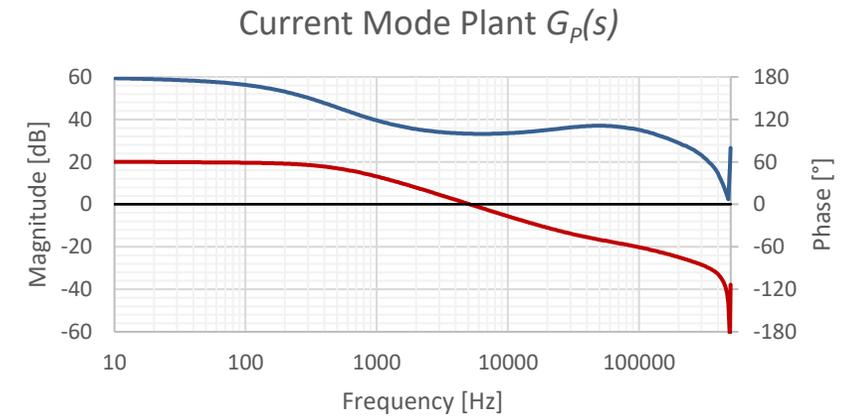
The average current feedback loop is established by cascading a dedicated voltage and current loop compensator, each tied to its respective feedback signal. Just like in peak current mode control, the outer voltage loop compensator output provides the reference for the inner current loop, where a second compensation filter adjusts the average inductor current by adjusting the modulated switch node control signal.

# Digital Control Scheme ACMC

## Step 1: Single Current Loop Controller

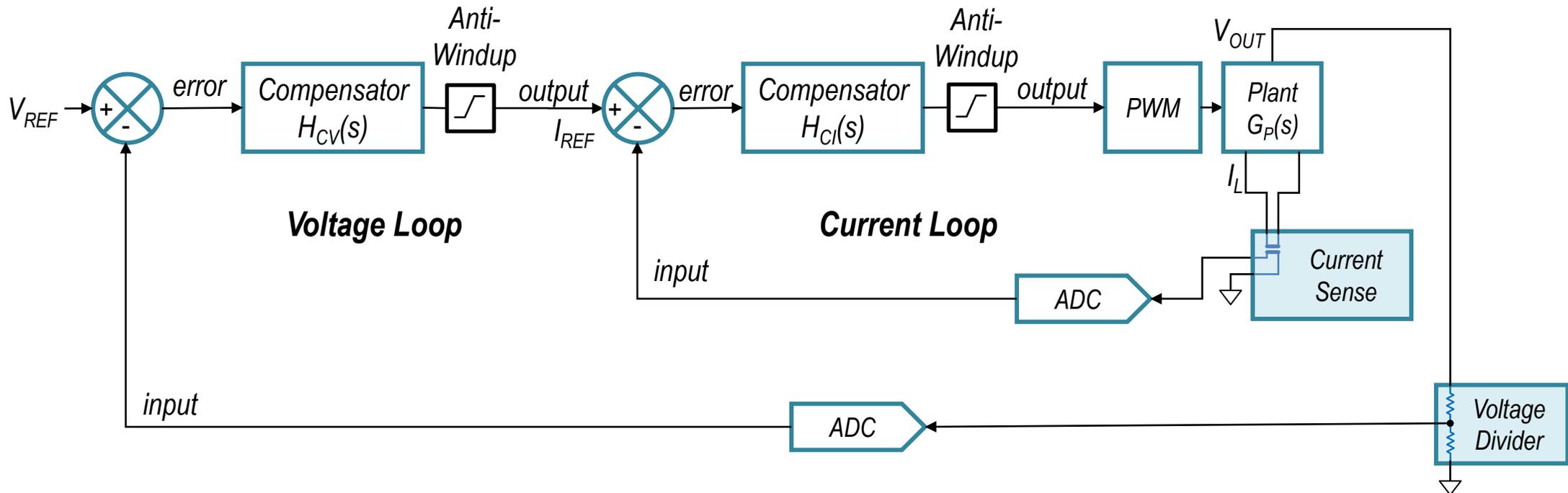


When we measure the inner current loop, we find the current mode plant transfer function being almost identical to its peak current mode counterpart, mainly shaped by one dominant plant pole.



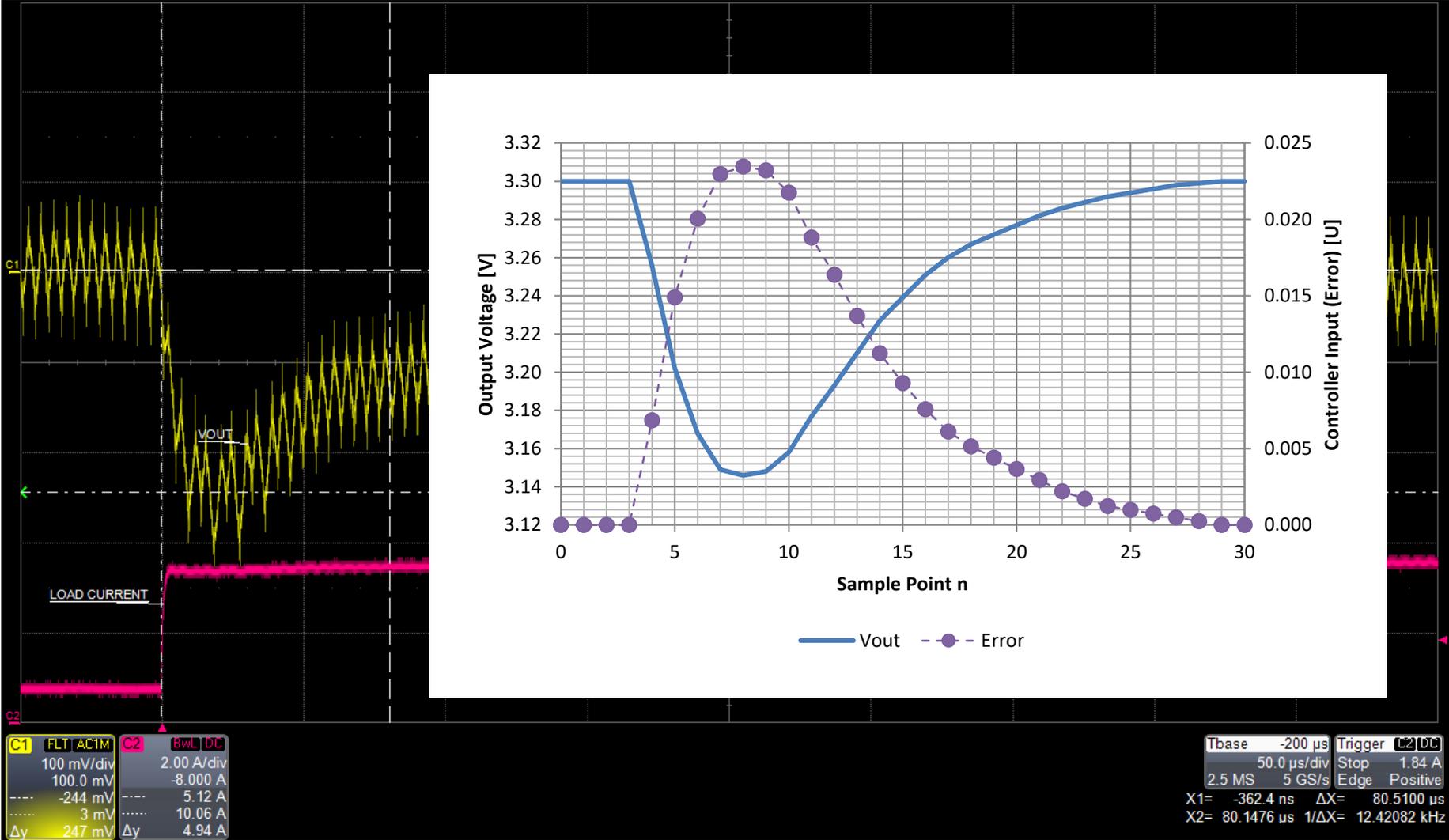
# Digital Control Scheme ACMC

## Step #2: Closing the Voltage Loop



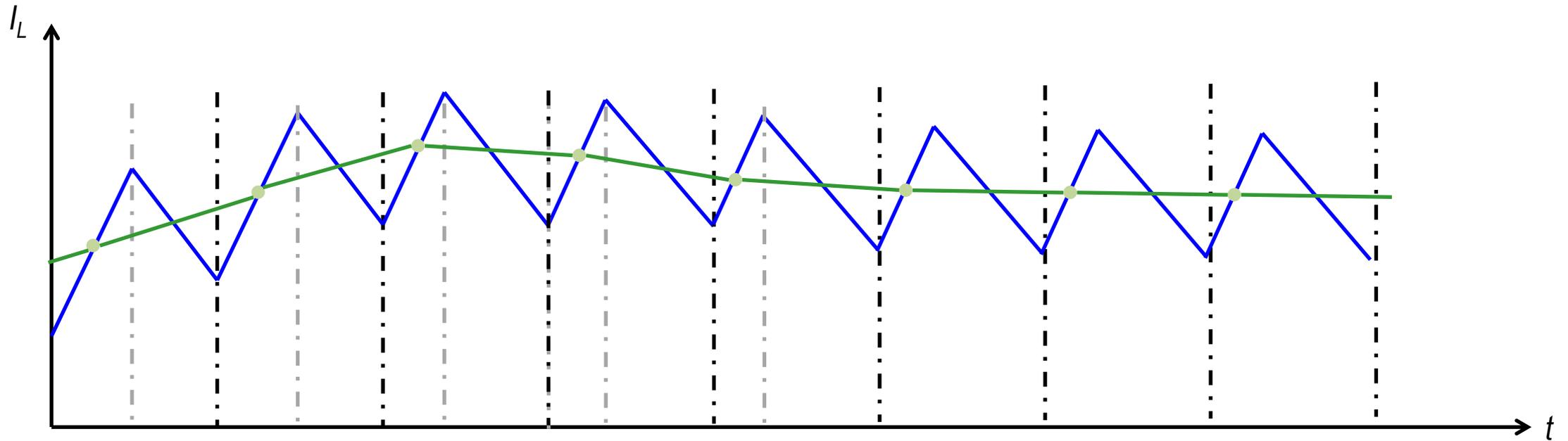
# Average Current Mode Step Response

## Control Loop Response vs. Output Voltage



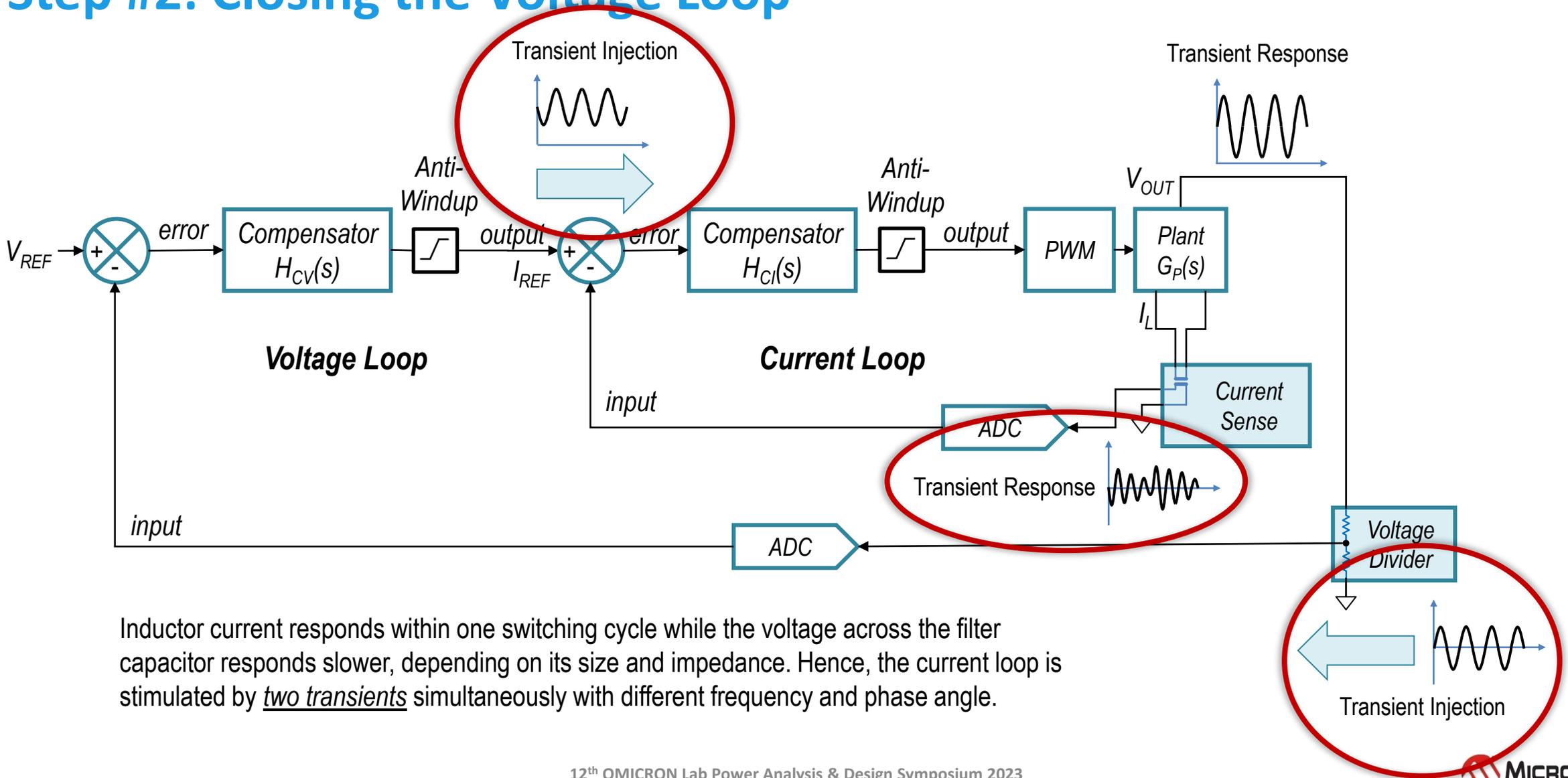
# Average Current Mode Step Response

## Control Loop Current Response



# Digital Control Scheme ACMC

## Step #2: Closing the Voltage Loop

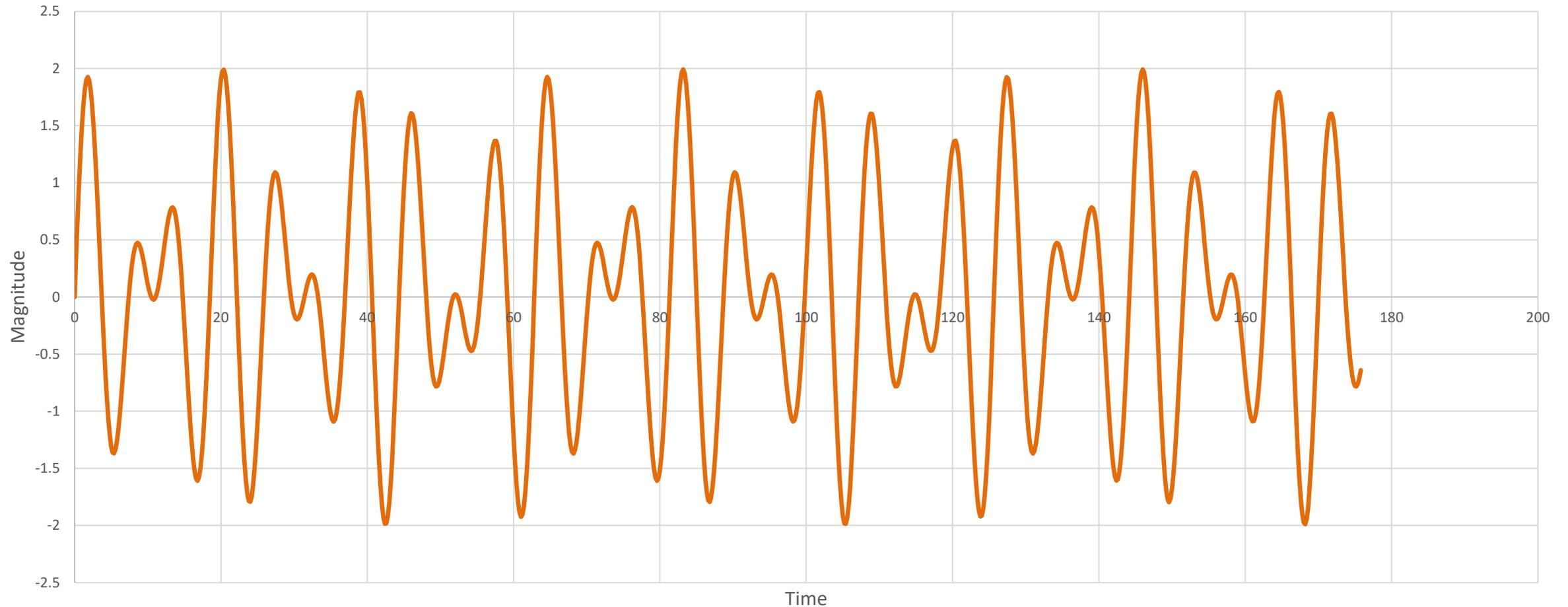


Inductor current responds within one switching cycle while the voltage across the filter capacitor responds slower, depending on its size and impedance. Hence, the current loop is stimulated by two transients simultaneously with different frequency and phase angle.

# Current Loop Transient Profile

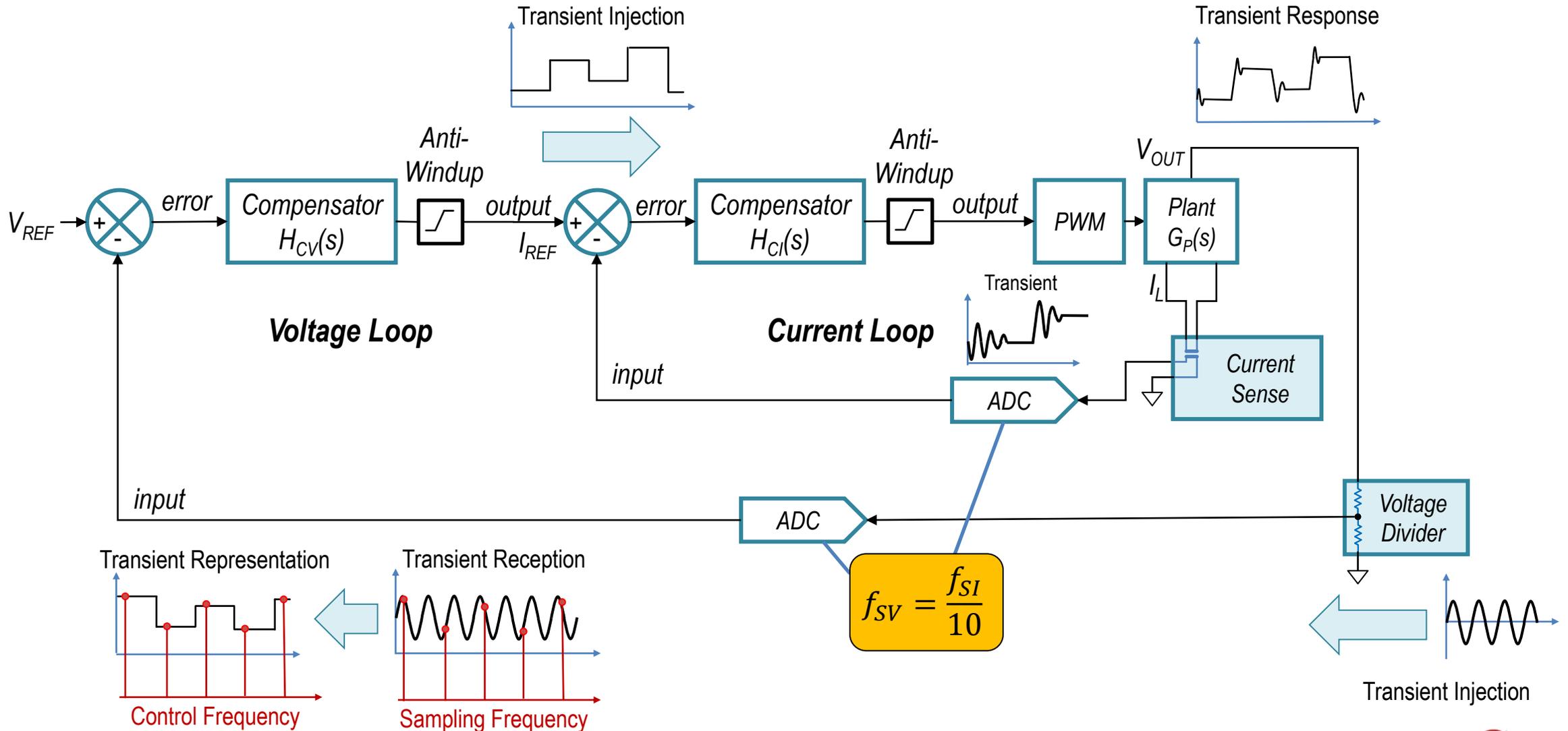
Transient signal waveform when stimulated on Reference and Feedback

Transient Frequency seen by Current Loop



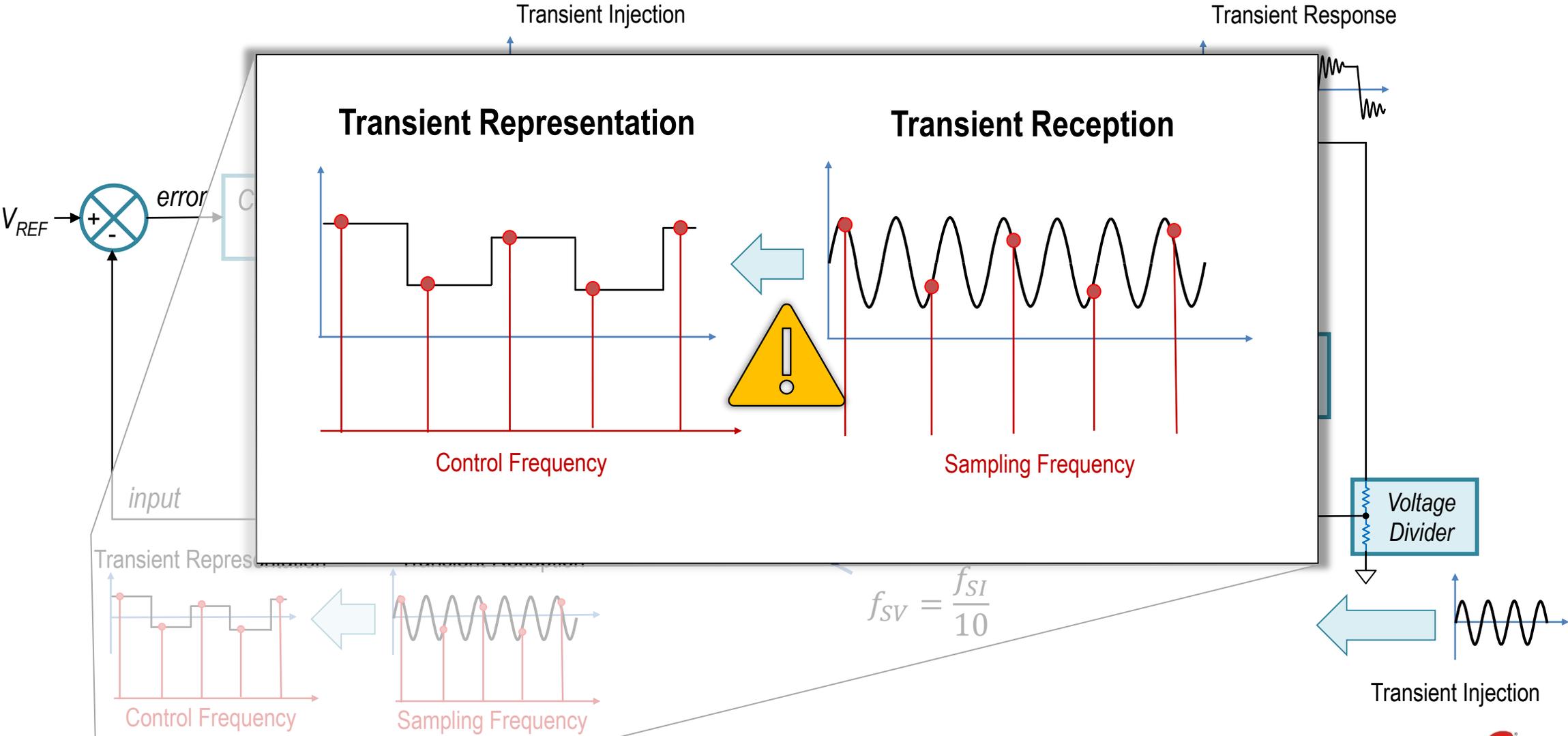
# Voltage-to-Current Loop Synchronization

## Approach #1: Sample Frequency Decoupling

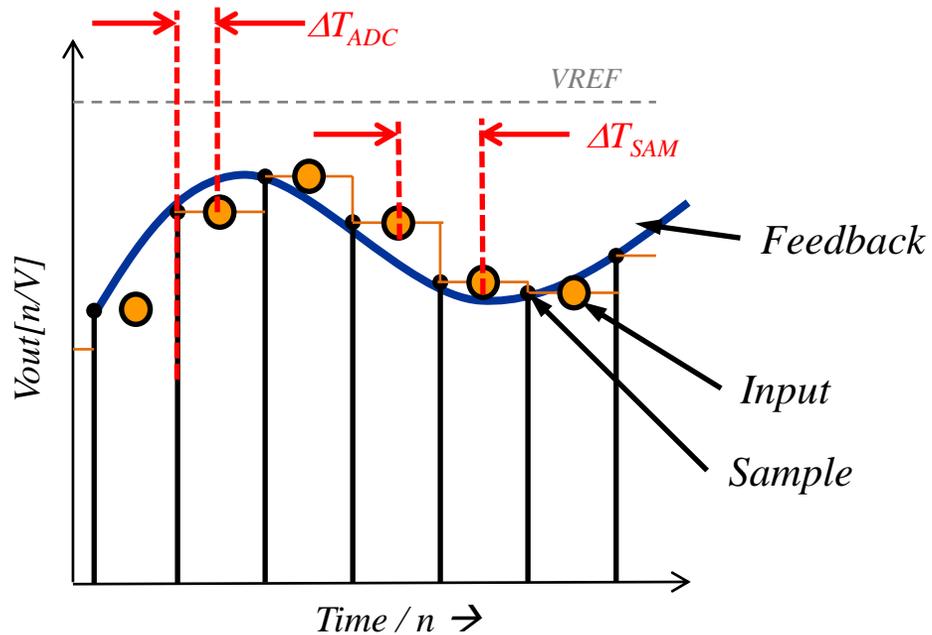


# Voltage-to-Current Loop Synchronization

## Approach #1: Sample Frequency Decoupling



# Discrete Time Domain Data Acquisition

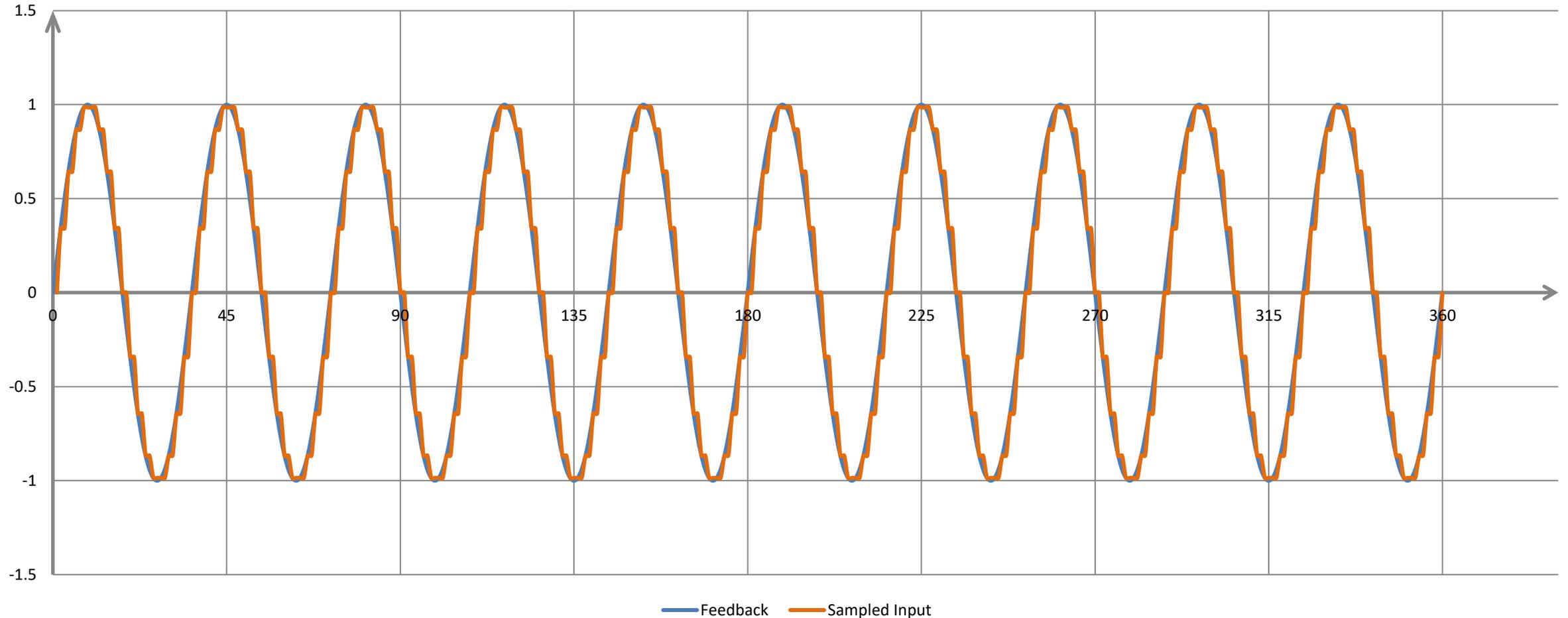


- The acquired signal is represented in “instantaneous” steps
- Signal sampling and conversion invokes phase shift
- The last sample is valid until it is updated by the next sample

# Alias Frequencies

Sufficient Oversampling Ratio (Alias-free Result)

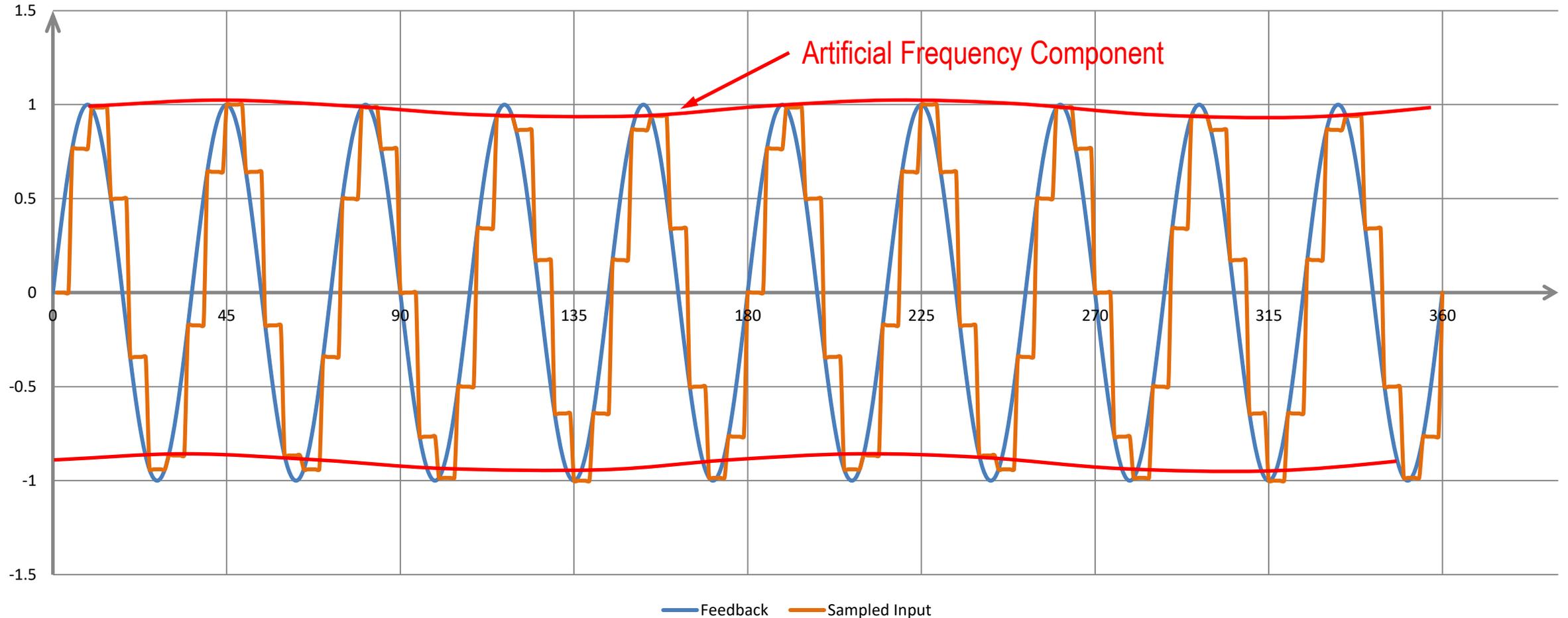
Waveform sampled at  $18 \times f_{IN}$



# Alias Frequencies

First Visible Sub-Frequency Component @  $f_{IN} \approx 1/8^{th}$  of  $f_{SAMPLE}$

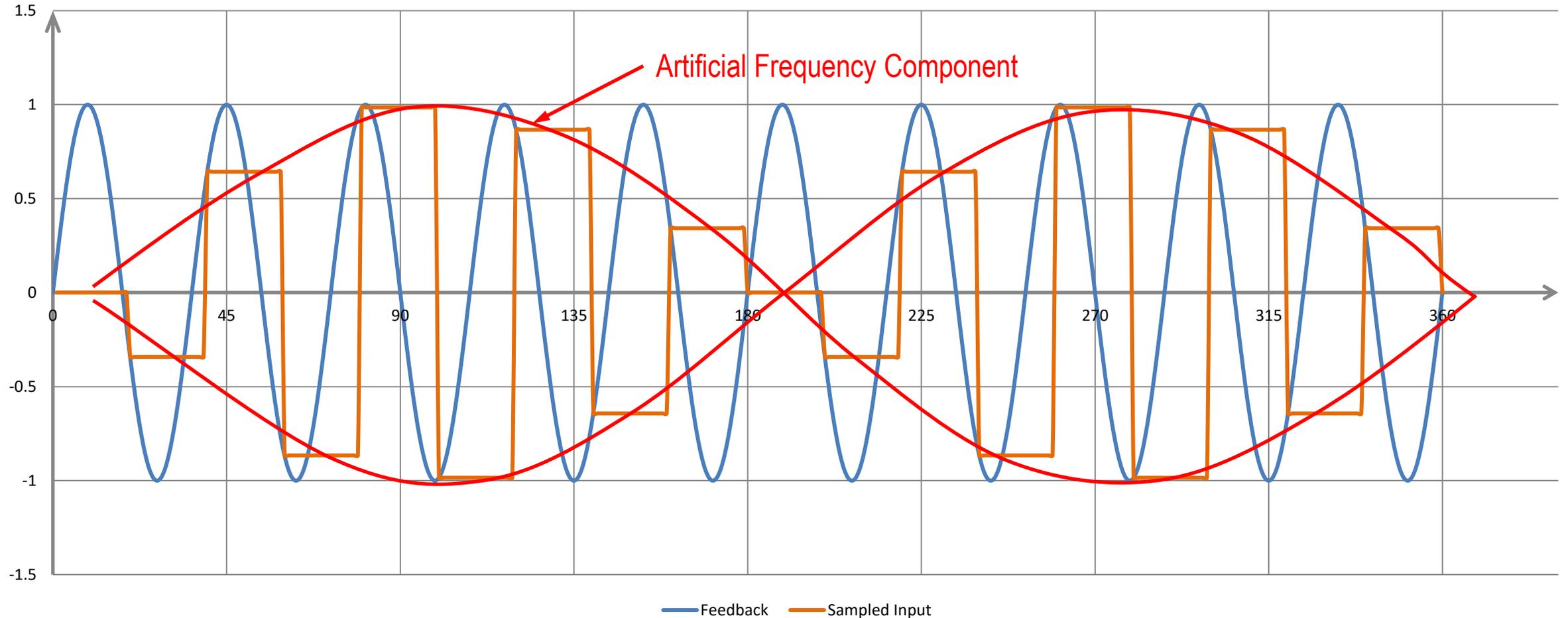
Waveform sampled at  $8x f_{IN}$



# Aliasing

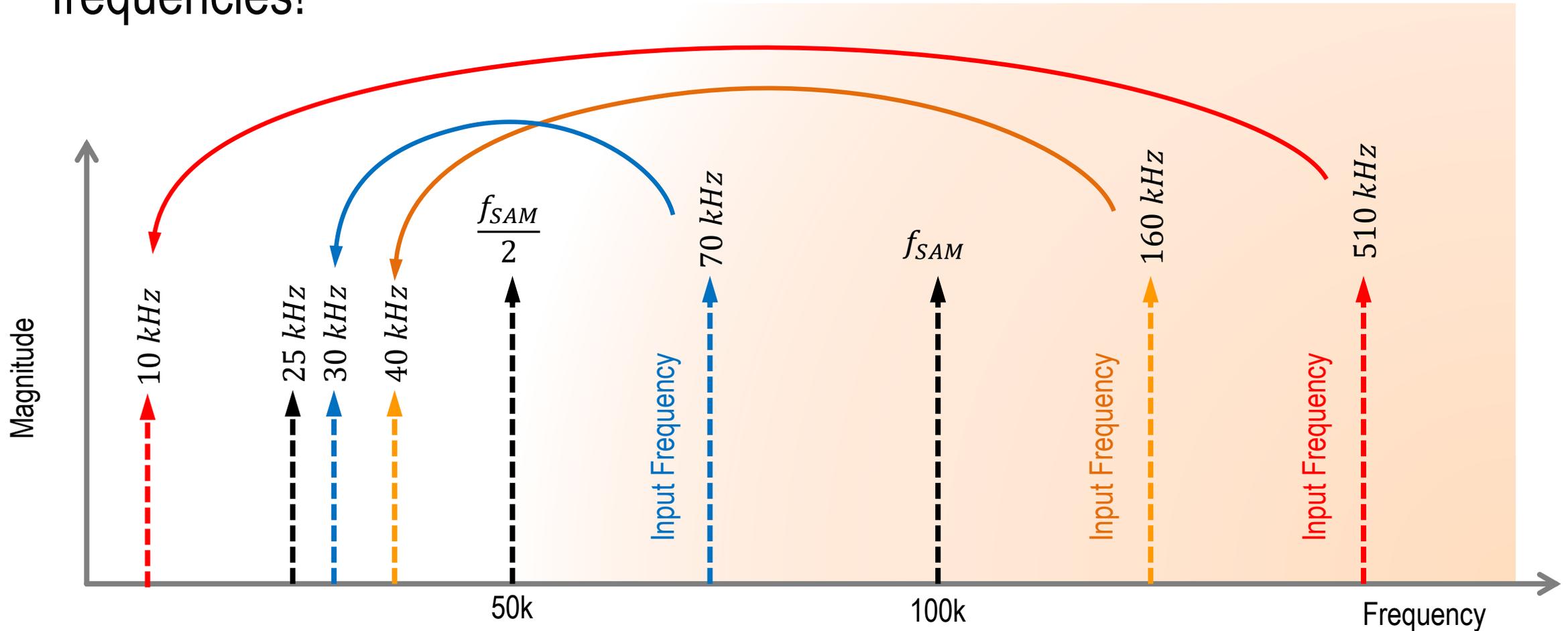
Highly distorted Result @  $f_{IN} = f_{NYQUIST} = \frac{1}{2}$  of  $f_{SAMPLE}$

Waveform sampled at  $2x f_{IN}$



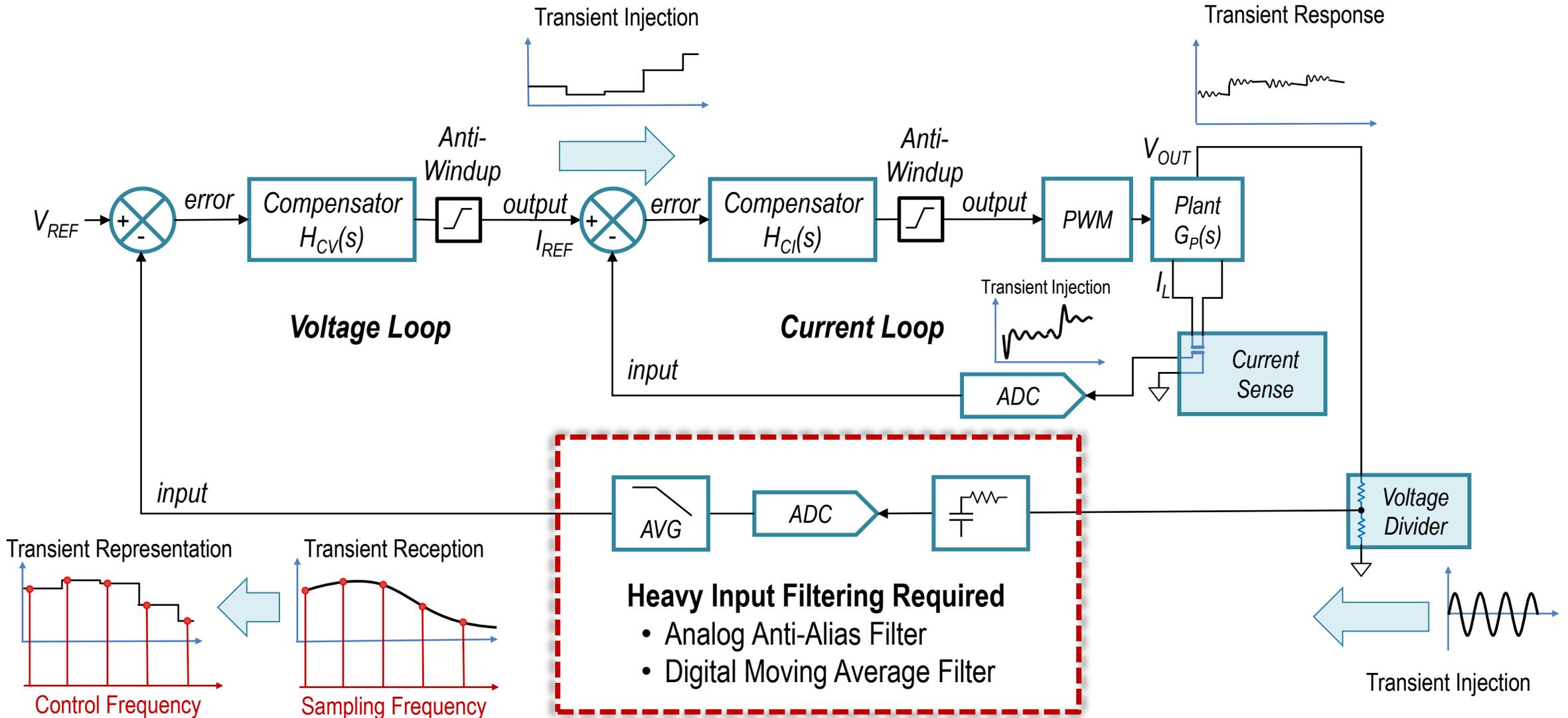
# Aliasing Example

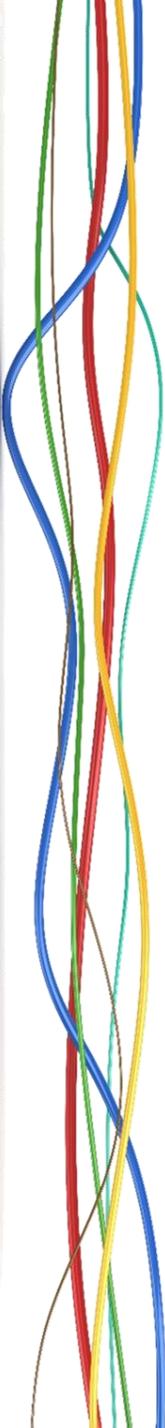
- Once injected, alias frequencies cannot be distinguished from real frequencies!



# Voltage-to-Current Loop Synchronization

## Approach #1: Sample Frequency Decoupling





# Voltage-to-Current Loop Synchronization

## Approach #1: Sample Frequency Decoupling

- **Challenges**

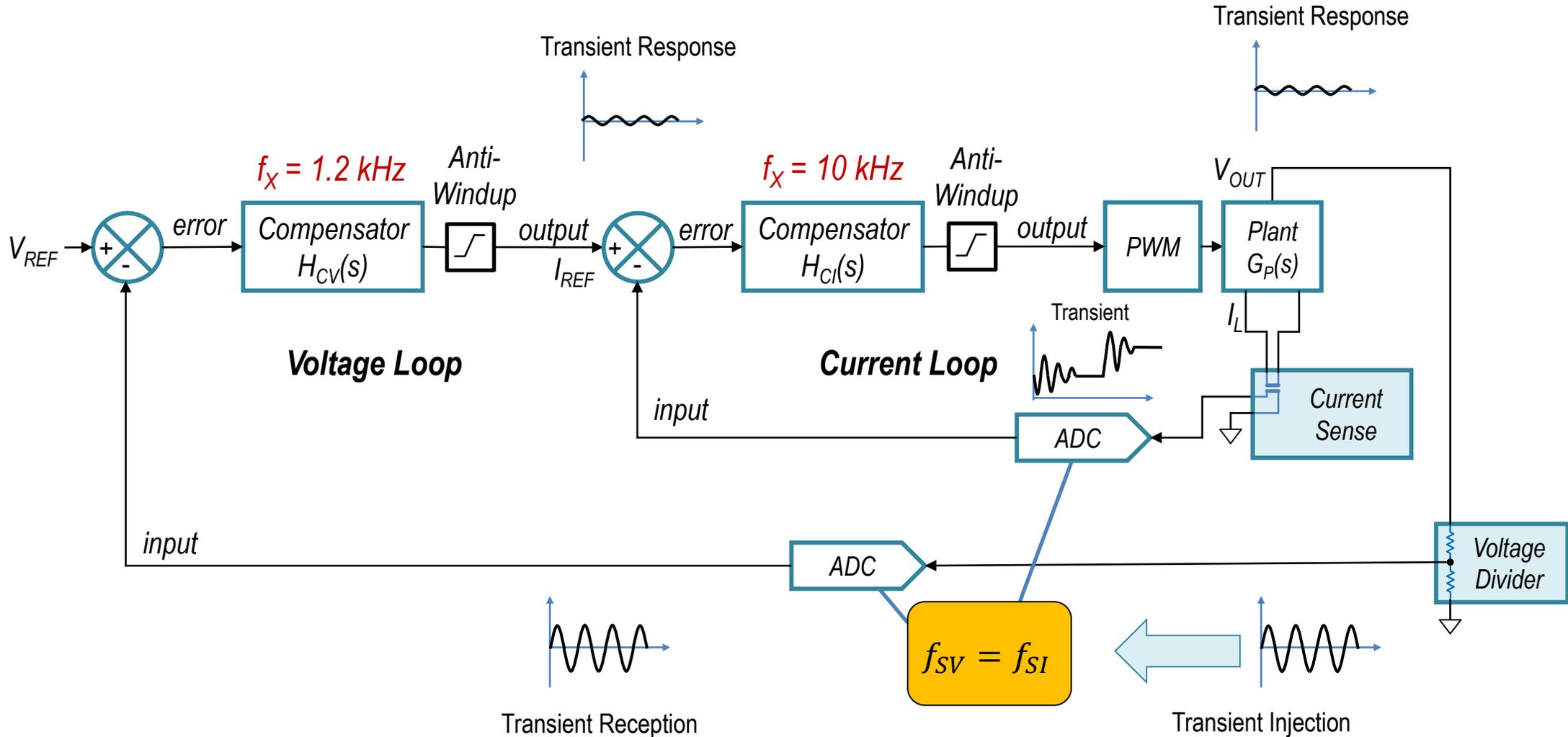
- Fast current response injects noise into voltage feedback
- High frequency noise must be filtered preventing alias frequencies from affecting the voltage loop, making the voltage loop even slower
- Slow voltage loop response injects step artefacts into output voltage
- **Low bandwidth response**

- **Applicable**

- Driving large capacitive loads (e.g. battery chargers)
- Power Factor Correction

# Voltage-to-Current Loop Synchronization

## Approach #2: Low Gain Voltage Loop

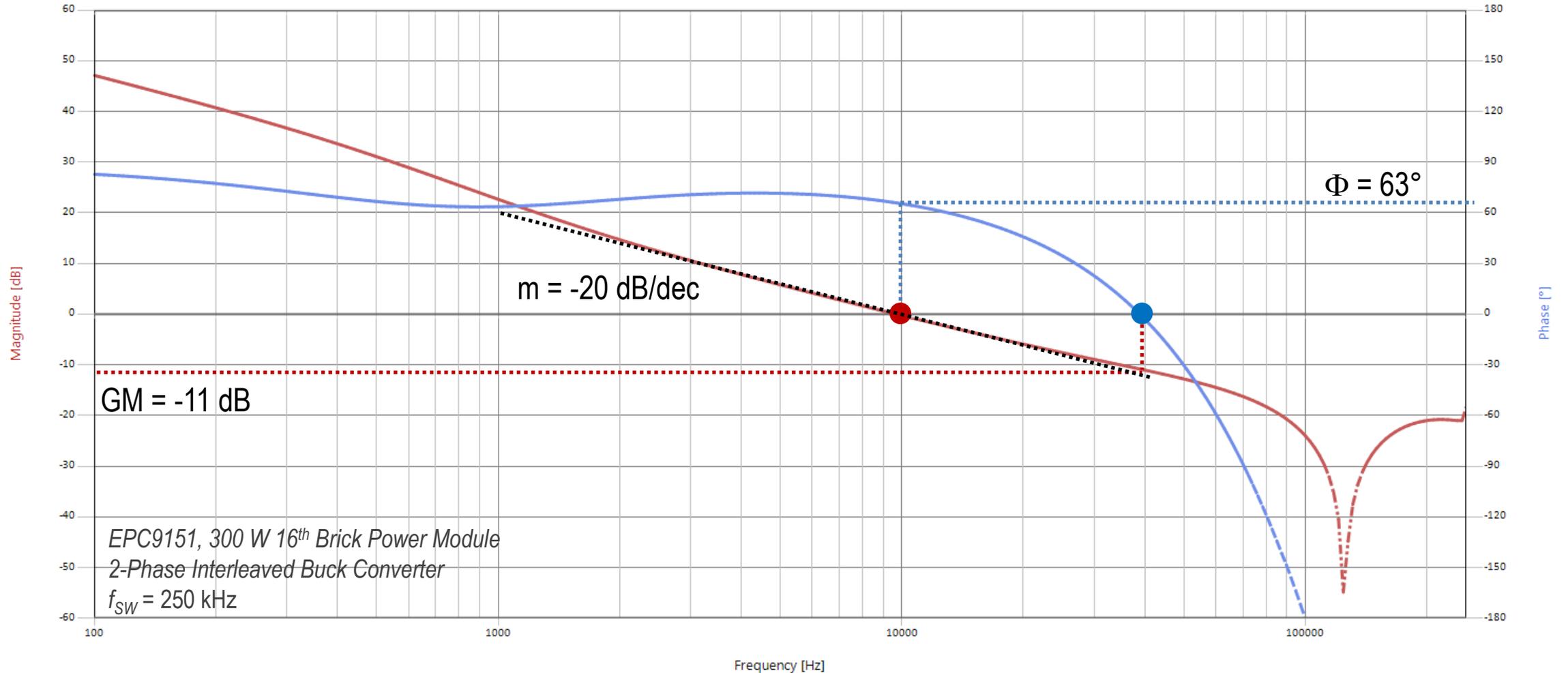


# Voltage-to-Current Loop Synchronization

Fast Inner Current Loop Open Loop Transfer Function ( $f_x = 10$  kHz)

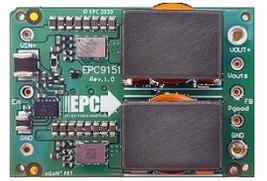


EPC9151  
300 W 16<sup>th</sup> Brick  
Interleaved Buck Converter

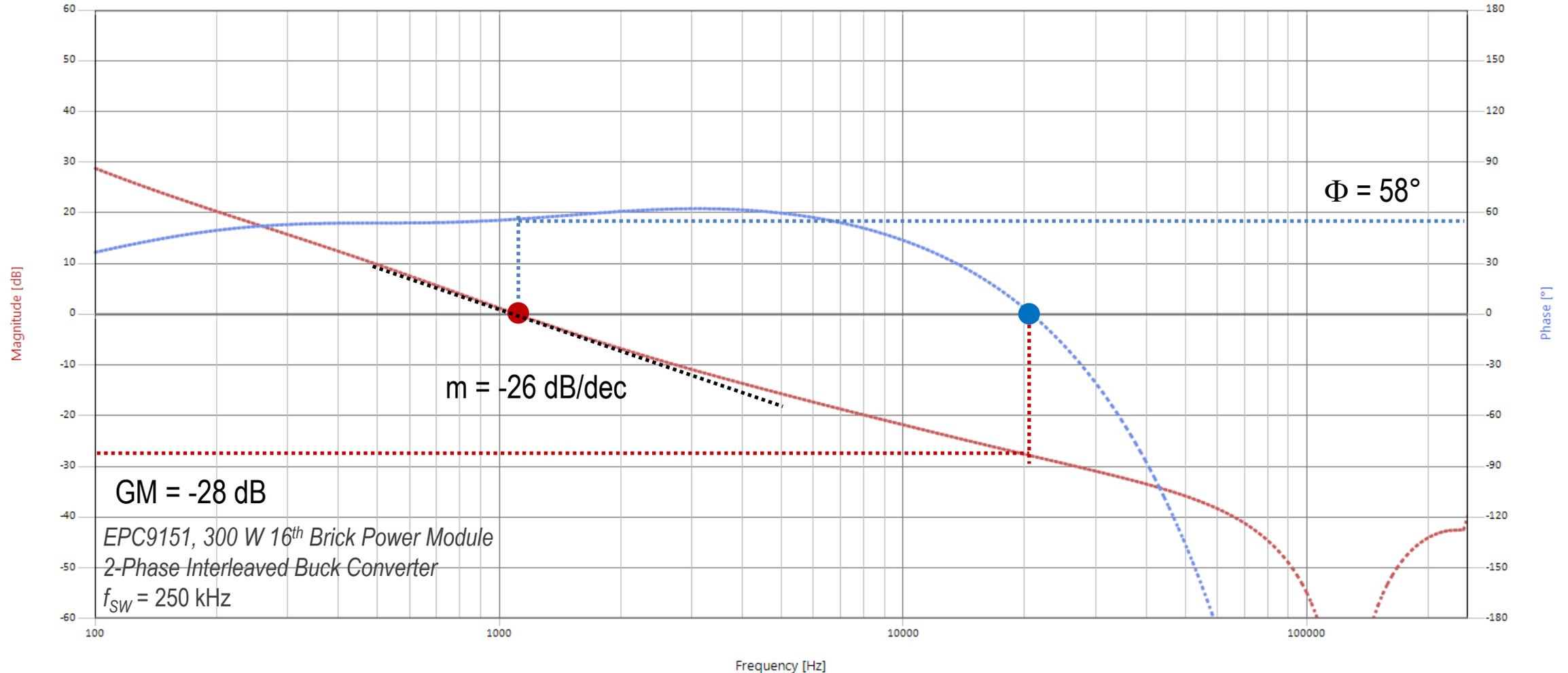


# Voltage-to-Current Loop Synchronization

Slow Outer Voltage Loop Open Loop Transfer Function ( $f_x = 1.2$  kHz)



EPC9151  
300 W 16<sup>th</sup> Brick  
Interleaved Buck Converter





# Voltage-to-Current Loop Synchronization

## Approach #2: Low Gain Voltage Loop

- **Results**

- Very good high frequency noise rejection without additional filtering
- Minimum perturbation of current reference
- **Low bandwidth response**

- **Applicable**

- Battery chargers
- LED Drivers
- Low-Performance DC/DC Converters
- Power Factor Correction

# Agenda



Power Supply Control Modes



Average Current Mode Control Implementation



Enforced Phase-Locking Method



Summary

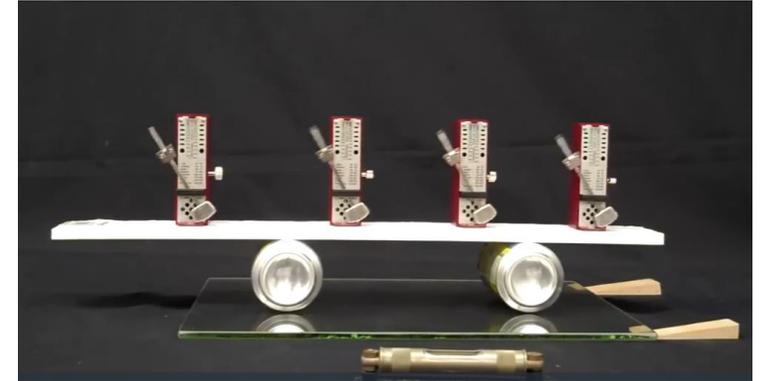
# Kuramoto Synchronization \*

## Approach #3: Enforced Phase-Locking Method

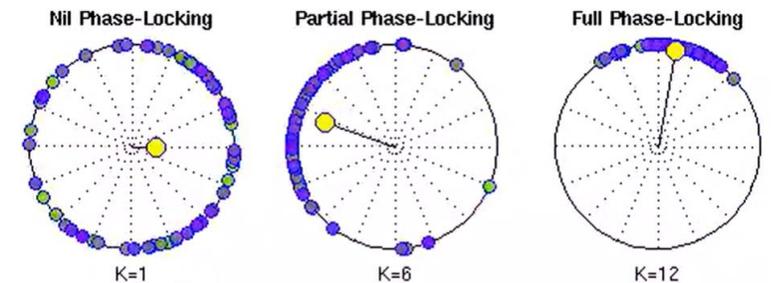
- \*This is not a Kuramoto model implementation but warm Thank You to Yoshiki Kuramoto for pointing us into the right direction
- And to [OMICRON Lab](#) giving us the tool we needed to work out how to implement it 😊



- The Kuramoto model in [Mechanics](#) describes the synchronization of a large set of coupled oscillators.
- **Famous example:** self-synchronization of metronomes swinging at different frequencies being forced into synchronization by being coupled through a moving base.



Kuramoto Oscillators



Nil, partial and full phase-locking in an all-to-all network of Kuramoto oscillators. Phase-locking is governed by the coupling strength  $K$  and the distribution of intrinsic frequencies  $\omega$ . Here, the intrinsic frequencies were drawn from a normal distribution ( $M=0.5\text{Hz}$ ,  $SD=0.5\text{Hz}$ ). The yellow disk marks the phase centroid. Its radius is a measure of coherence.

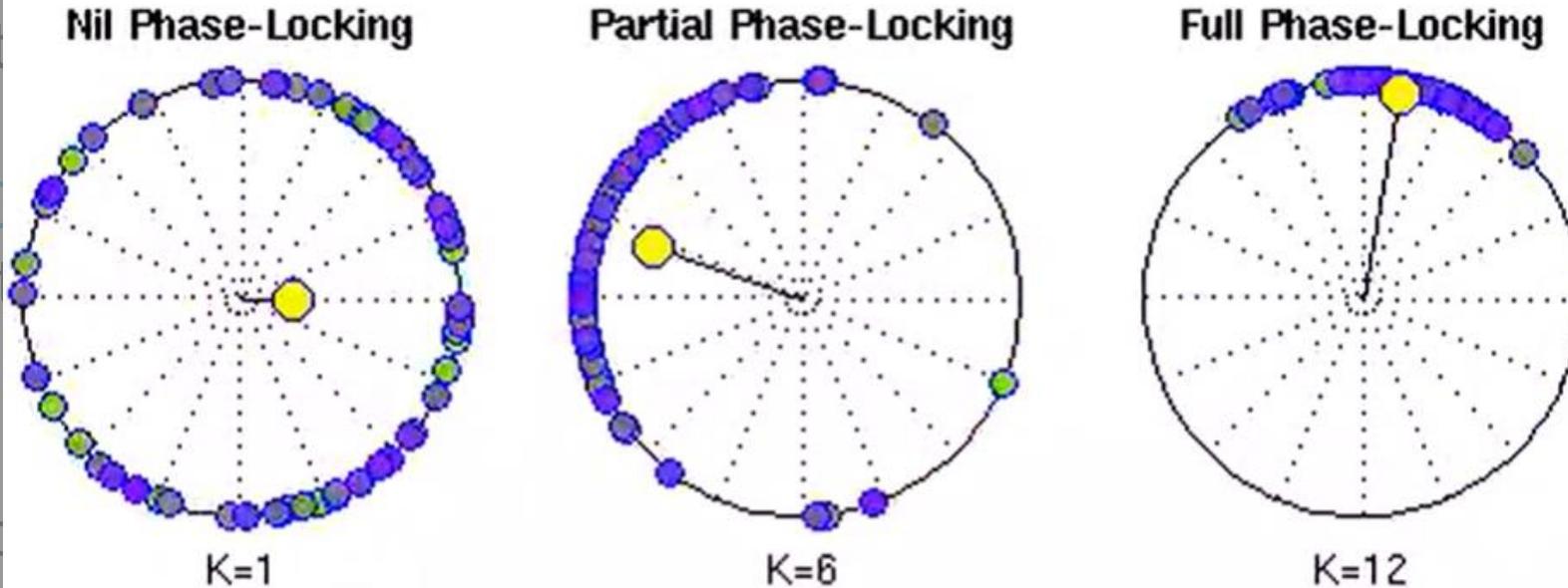
# “Kuramoto” Synchronization\*

## Approach #1

- \*This is *not* a simple task. Thank You to the direction
- And to OMC for implementing it
- The Kuramoto synchronization
- Famous example of swinging at synchronization

## Kuramoto Oscillators

\*Screenshot of animation on Wikipedia



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## to Oscillators



In an all-to-all network of Kuramoto oscillators, phase-locking is governed by the coupling strength  $K$  and the distribution of intrinsic frequencies  $\omega$ . Here, the intrinsic frequencies were drawn from a normal distribution ( $M=0.5\text{Hz}$ ,  $SD=0.5\text{Hz}$ ). The yellow disk marks the phase centroid. Its radius is a measure of coherence.

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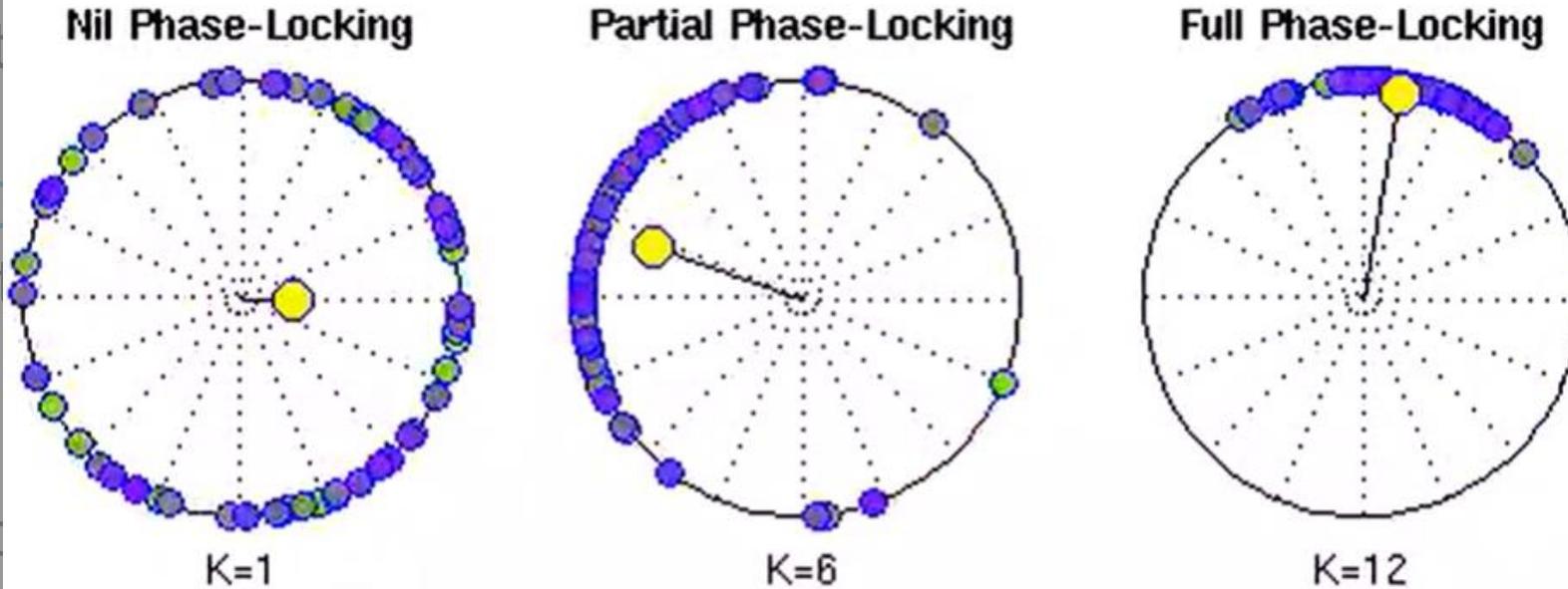
## Approach #1

- \*This is *not* a simple matter of connecting oscillators in a single direction
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- The Kuramoto synchronization
- Famous example of swinging at synchronization

## Kuramoto Oscillators

\*Screenshot of animation on Wikipedia



Nil, partial and full phase-locking in an all-to-all network of Kuramoto oscillators. Phase-locking is governed by the coupling strength  $K$  and the intrinsic frequencies  $\omega_i$ . Here, the intrinsic frequencies are  $M=0.5\text{Hz}$ ,  $SD=0.5\text{Hz}$ . The yellow dot is a measure of coherence.

Does not apply for power supplies as the plant is not a strong coupling medium.

**But is there another way to enforce full phase-locking?**



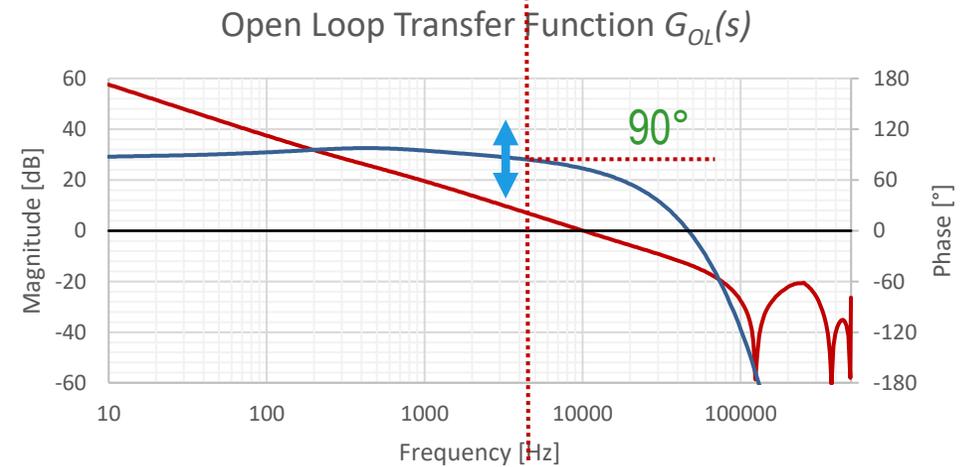
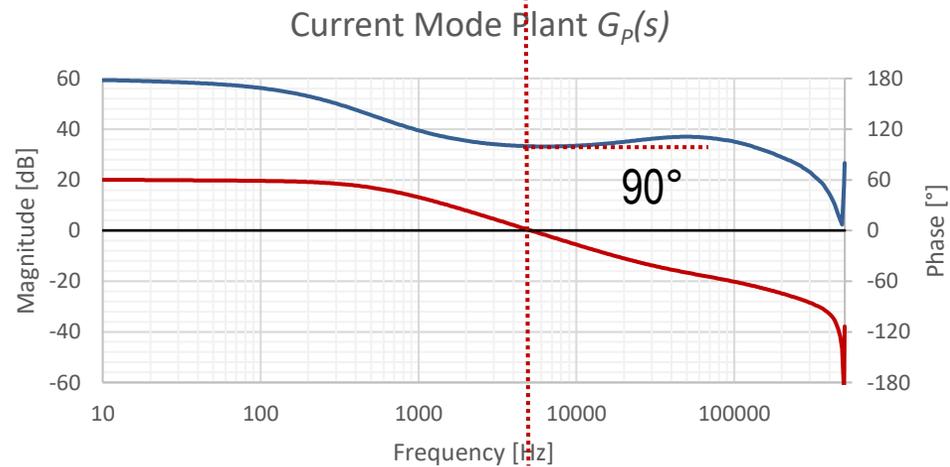
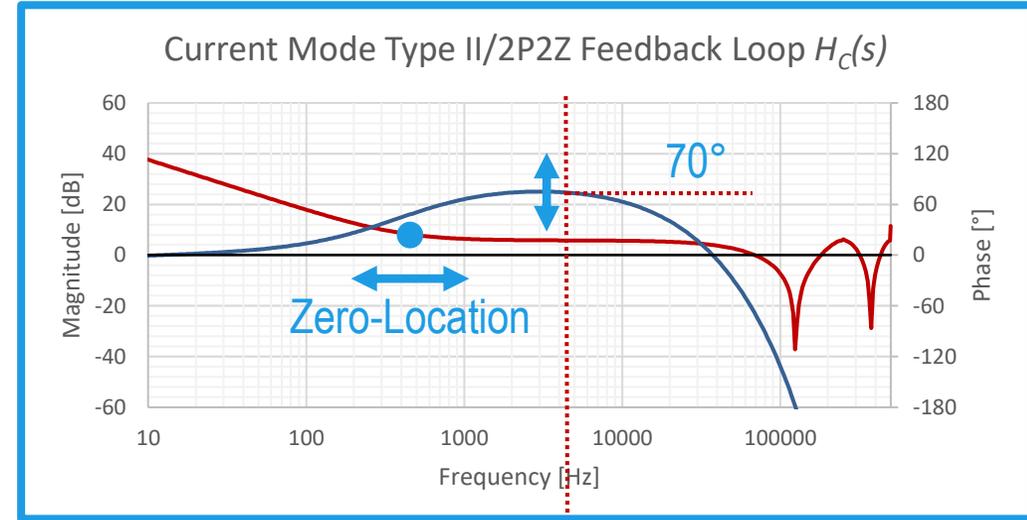
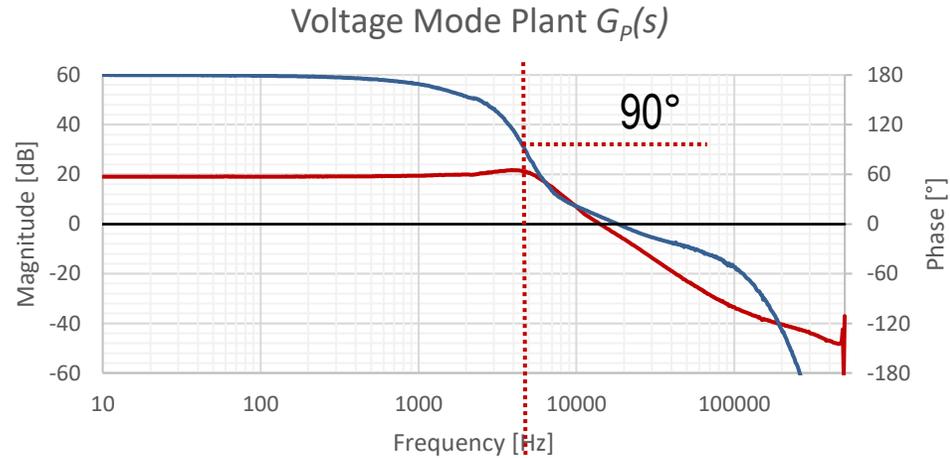
## Two Oscillators



In an all-to-all network of Kuramoto oscillators, the synchronization is governed by the coupling strength  $K$  and the intrinsic frequencies  $\omega_i$ . Here, the intrinsic frequencies are  $M=0.5\text{Hz}$ ,  $SD=0.5\text{Hz}$ . The yellow dot is a measure of coherence.

# Enforced Phase-Locking Method

## Inner Current Loop Tuning

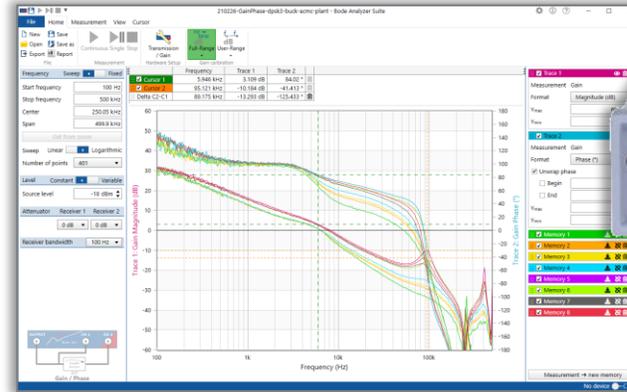
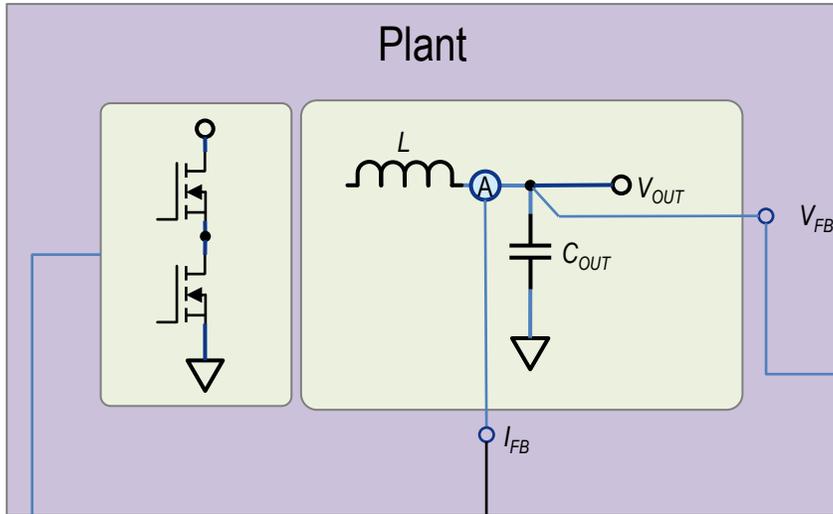


4.7 kHz

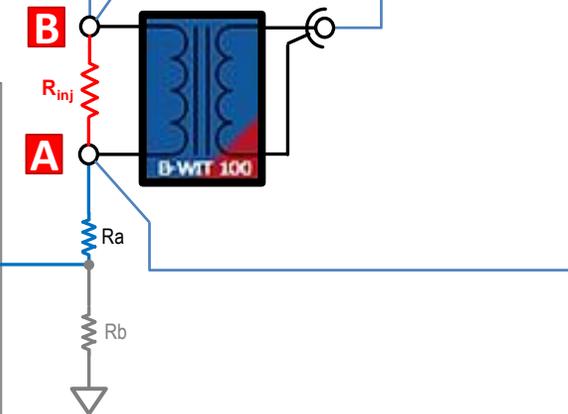
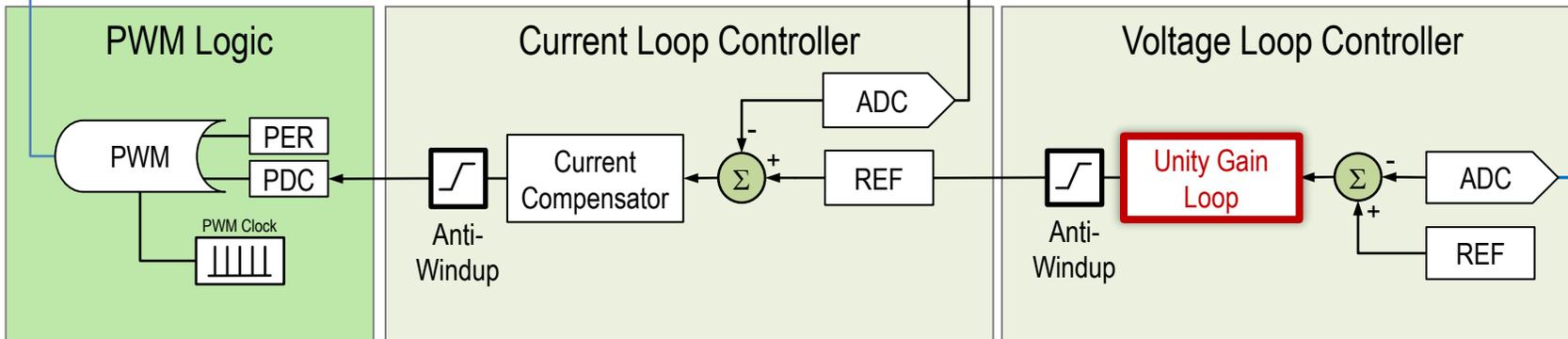
4.7 kHz

# Alternate Current Plant Measurement

## Current Plant seen from Voltage Loop

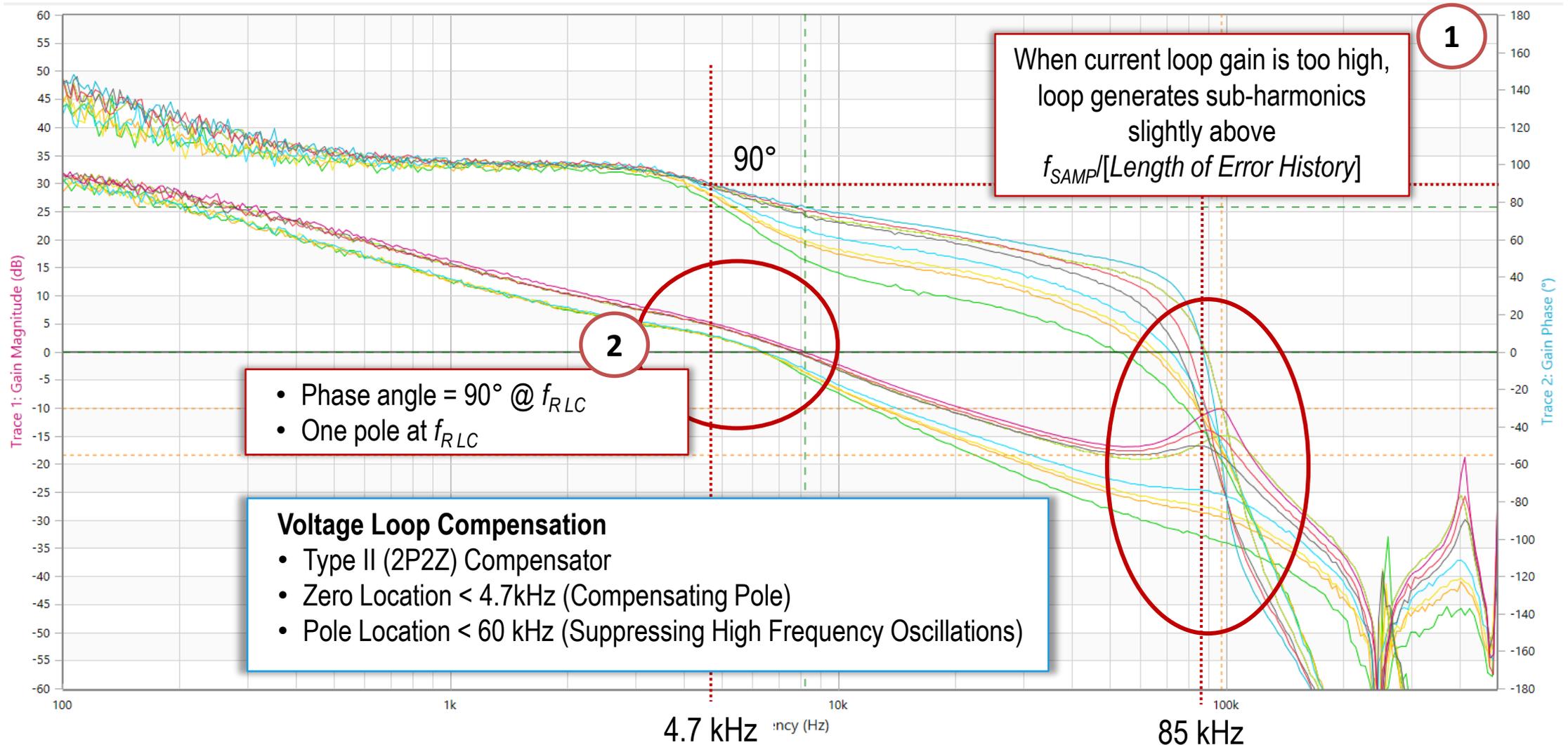


Unity Gain Loop makes voltage loop  
“transparent” but injects transients in  
current reference



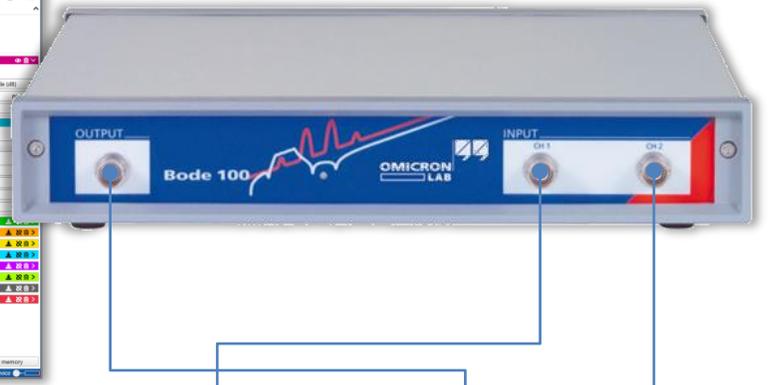
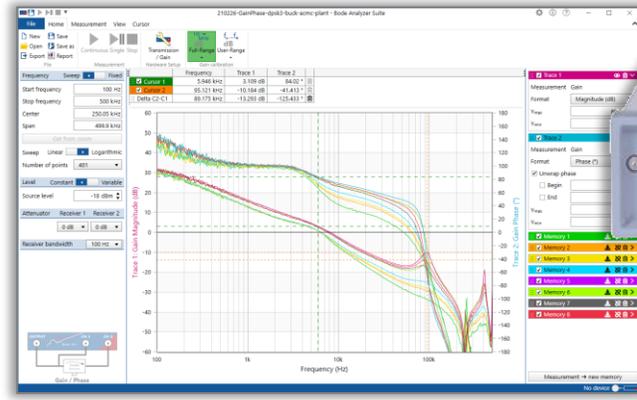
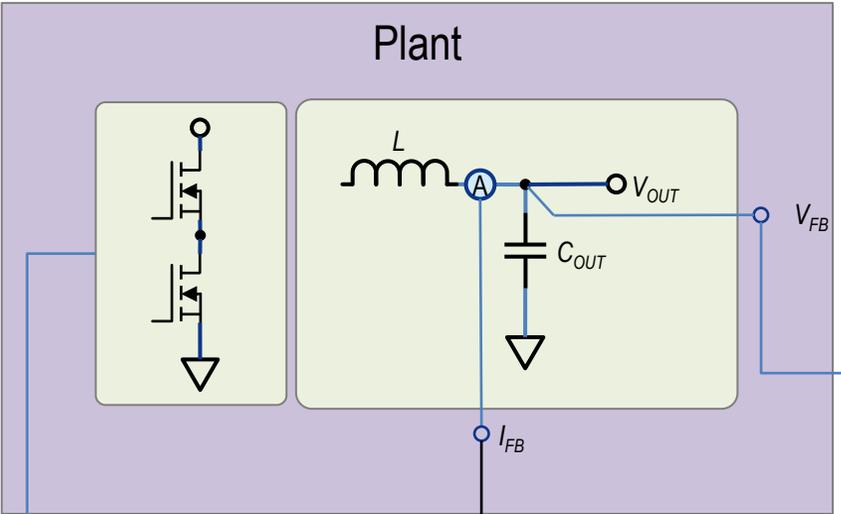
# Enforced Phase-Locking Method

## Results: Voltage Response of Current Loop Plant

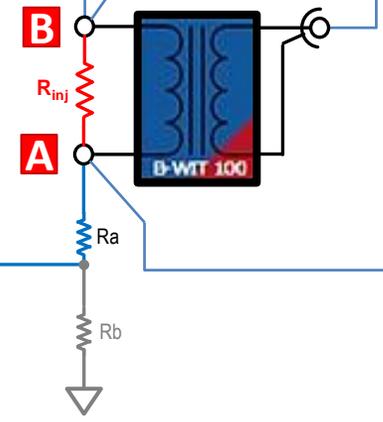
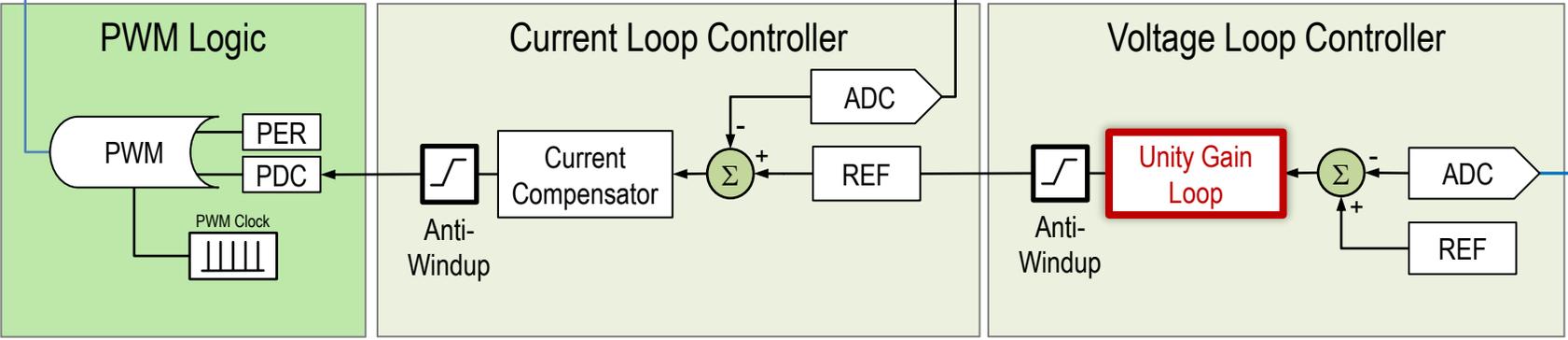


# Alternate Current Plant Measurement

## Current Plant seen from Voltage Loop

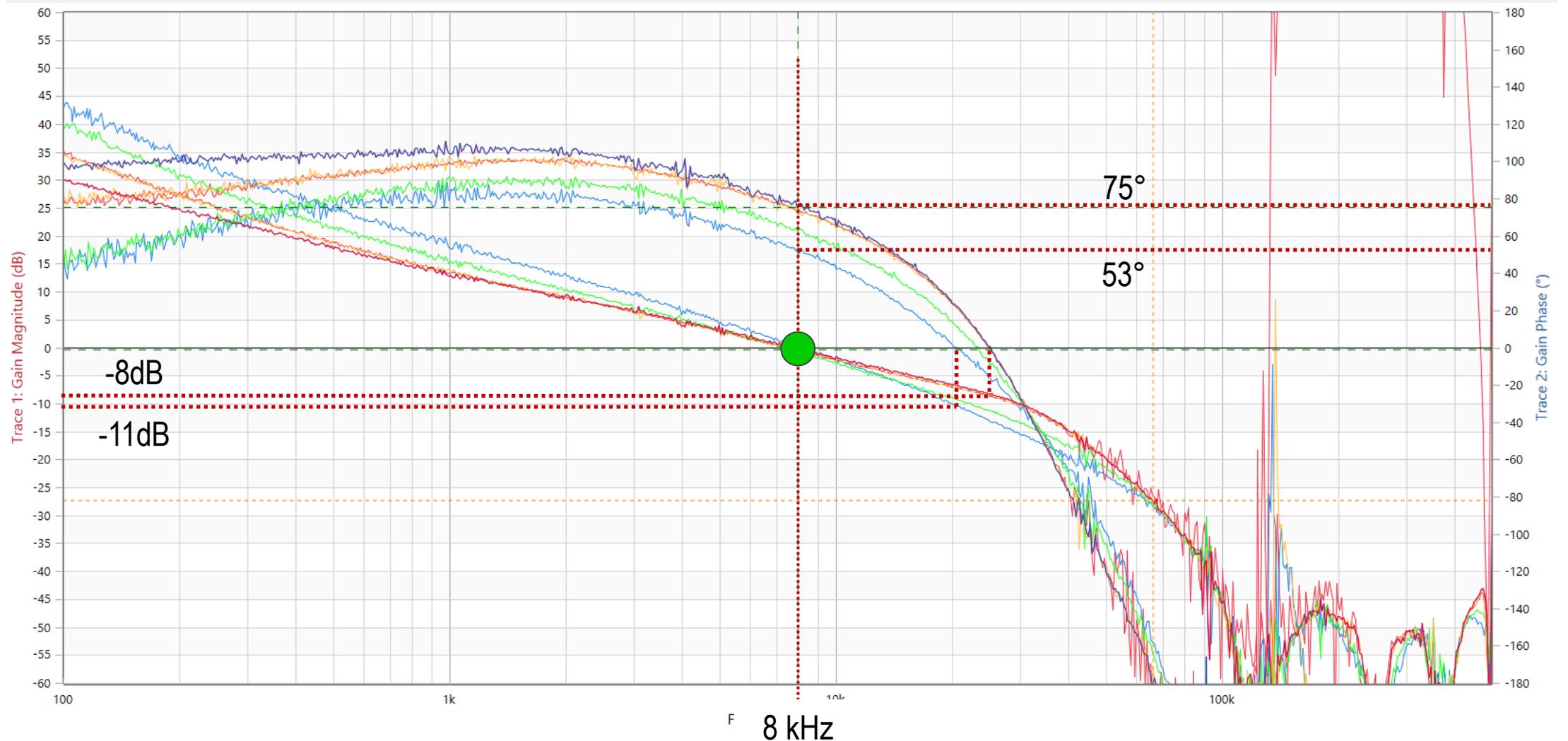


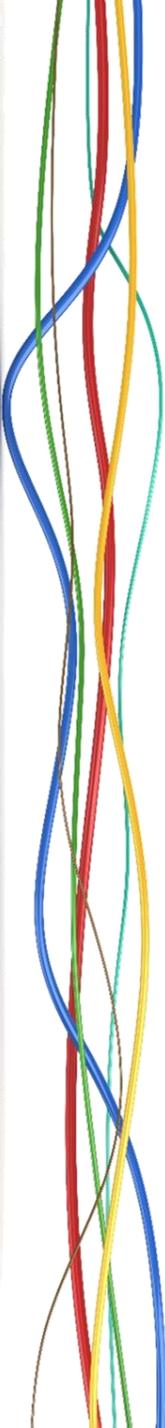
Unity Gain Loop makes voltage loop "transparent" but injects transients in current reference



# Enforced Phase-Locking Method

## Average Current Mode Control Open Loop Transfer Function Results





# Enforced Phase-Locking Method

## Wrap-Up

- **Most Recent Results**

- Enforced Phase-Locking of Voltage and Current loop result in a stable and reliable system
- As a result, Current Loop is **slower** than the Voltage Loop
- Until today, results only verified on forward-type converters with fast current sense circuits

- **Future Work**

- Evaluation of application in other topology types
- Evaluation of impact of current feedback bandwidth/phase shift limitations

# Agenda



Power Supply Control Modes



Average Current Mode Control Implementation



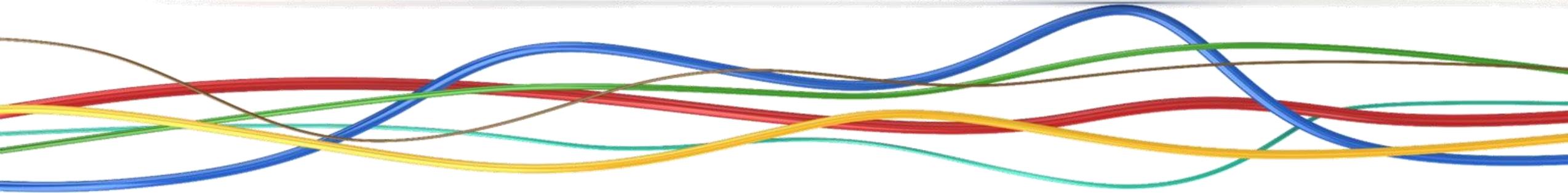
Enforced Phase-Locking Method



Summary

# Summary

- **Average Current Mode Control is a universal control mode applicable in**
  - Constant Current and Constant Voltage Sources
  - PFC and DC/DC Converters
  - Battery Chargers & LED Drivers
  - Allows current-oriented control algorithms (e.g. MPPT, Bidirectional Control)
  - Sustained Current Limit capability
- **Less restrictive on current feedback quality**  
(simplifies current sense circuits)
- **Higher CPU load in digital control loop implementations**
- **Classic configurations have limited bandwidth**
- **Promising: Phase-Locking may be key to mitigate bandwidth limitations**



# Q & A

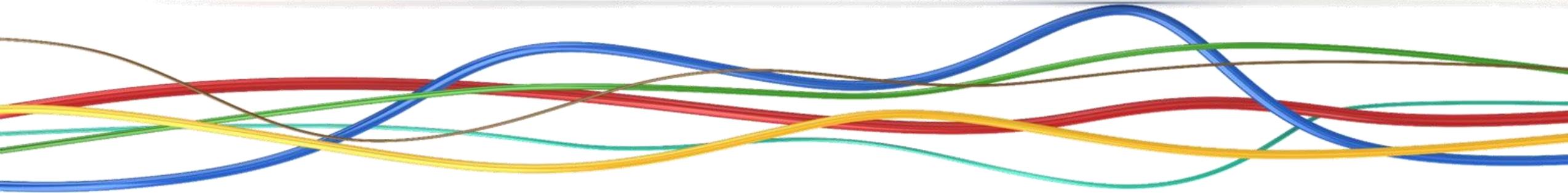
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# Thank You!

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May the power be with you!



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